OLD STATE ROAD
HAMBDEN TWP.

88

DIETZGEN

TRADE MARK

ENGINEERS'

LEVEL BOOK

No. 410

EUGE[illegible] ZGE[illegible] CO.

DRAWING MA[illegible] MATHEMATICAL and
SURVEYING [illegible]

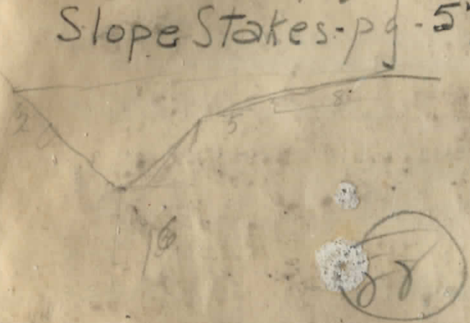
Chicago New York San Francisco New Orleans Pittsburg Toronto

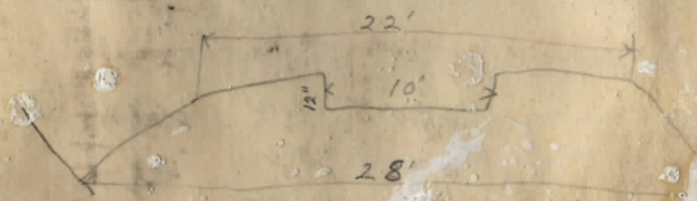
Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	19.8	10.9	2
3	[illegible]	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	[illegible]	[illegible]	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	[illegible]	[illegible]	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	[illegible]	[illegible]	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	[illegible]	[illegible]	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	[illegible]	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	[illegible]	[illegible]	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
[illegible]	[illegible]	18.1	[illegible]	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
[illegible]	[illegible]	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
[illegible]	[illegible]	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
[illegible]	[illegible]	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	[illegible]	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	[illegible]	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	24.7	[illegible]	24.9	16
17	25.0	[illegible]	[illegible]	[illegible]	[illegible]	25.5	[illegible]	[illegible]	[illegible]	25.9	17
18	26.0	26.1	26.2	26.3	26.4	[illegible]	26.6	[illegible]	[illegible]	[illegible]	18
19	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	19
[illegible]	28.0	28.1	28.2	[illegible]	28.4	[illegible]	[illegible]	[illegible]	28.8	28.9	20
21	29.0	29.1	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	29.8	29.9	21
22	30.0	30.1	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	30.8	30.9	22
23	31.0	31.1	31.2	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	31.8	31.9	23
24	32.0	32.1	32.2	[illegible]	32.4	[illegible]	[illegible]	32.7	32.8	32.9	24
25	33.0	33.1	[illegible]	[illegible]	[illegible]	33.5	[illegible]	[illegible]	33.8	33.9	25
26	34.0	34.1	34.2	[illegible]	34.4	34.5	[illegible]	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	[illegible]	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	[illegible]	41.2	[illegible]	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	[illegible]	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	[illegible]	[illegible]	43.4	43.5	43.6	43.7	43.8	43.9	35
[illegible]	44.0	44.1	44.2	[illegible]	44.4	[illegible]	44.6	44.7	44.8	44.9	36
[illegible]	45.0	45.1	[illegible]	45.3	45.4	[illegible]	45.6	45.7	45.8	45.9	37
[illegible]	46.0	[illegible]	[illegible]	[illegible]	46.4	46.5	46.6	[illegible]	[illegible]	46.9	38
[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	47.5	47.6	[illegible]	47.8	47.9	39
40	48.0	[illegible]	[illegible]	48.3	[illegible]	48.5	[illegible]	[illegible]	[illegible]	48.9	40

[illegible]—If [illegible] is 22.6 ft. above grade, how far [illegible] it be from center line [illegible] point? Ans. from table 30.6. For same slope [illegible] other widths [illegible] correct above figures by one-half difference in width [illegible], thus in [illegible] for 20 ft. roadbed distance will be 30.6 + (20— [illegible] added to [illegible] of 1 or 1½ see inside of back cover.

OLD STATE ROAD
HAMBDEN TWP.





Deep Snow.

Jan. 6, 1925, Fair, 30°

Marks + Gray

			1288.45
			1316.14
			1187.78
10.19	1298.64		1288.45
7.38	1305.99	0.03	1298.61
0.29	1303.52	2.76	1303.23
0.03	1298.39	5.16	1298.36
		5.34	1293.05
0.47	1286.84	11.92	1286.47
0.32	1274.72	12.54	1274.40
		8.09	1266.63
7.85	1271.32	11.25	1263.47
0.27	1264.88	6.71	1264.61
3.86	1258.03	10.71	1254.17
1.73	1258.81	0.95	1257.08
10.55	1269.36	0.00	1258.81
5.52	1274.73	0.15	1269.21
		9.10	1265.63
9.94	1284.34	0.33	1274.40
11.46	1295.47	6.33	1284.01

B.M. S.E. cor. S.H.W. Culvert 200' W. of Chamberlains 1300' W. of State Road

B.M. S.E. Cor. S. Head-Wall Culvert at Hambden School

B.M. Staple, N.E. Root, 36" Elm S.W. of Lamp mars. Corners

B.M. S.E. Cor. E.H.W. 1300' W. of Old State Rd on N. Hambden St.

B.M. set, N.E. Root 15" Maple, S.W. Cor. Old State Rd. N. Hambden St.

B.M. set. S.W. Root, 30" Maple, Rt. ~~134+35~~ 135+35

B.M. set, S.W. Root 24" Maple Rt. ~~126+35~~ 127+35

~~B.M. set, W. root, 18" Hem~~

B.M. Set, W. root, 20" Hemlock, Rt. 10~~7~~+75

B.M. set. E. root, 30" Maple, Left 9~~3~~+20

	1295.47		
12.28	1307.75	0.00	1295.47
7.79	1315.54	0.00	1307.75
		6.47	1309.07
0.73	1312.38	3.89	1311.65
0.70	1303.91	9.17	1303.21
0.47	1291.65	12.73	1291.18
		8.54	1283.11
0.02	1279.35	12.32	1279.33
2.42	1270.62	11.15	1268.20
8.91	1261.51	10.02	1260.60
1.84	1252.54	10.81	1250.70
		3.10	1249.44
1.88	1245.37	9.05	1243.49
0.83	1234.25	11.95	1233.42
		10.27	1223.98
9.53	1233.51		1223.98
8.86	1242.37	0.00	1233.51
0.45	1230.93	11.89	1230.48
1.12	1219.62	12.43	1218.50

B.M. set, W. root, large Elm, R+79+75

B.M. Set W. root, 30" Maple, Rt, 61+30

B.M. Set, N.E. root 18" Maple Lt, 41+60

B.M. set, Spike at R.P.-S.W. side 2nd 15" Maple S. of Corners con E. side
Jan. 7, 1925, Fair, Deep Snow. 30° Marks Gray

	1219.62		
		0.41	1219.21
0.73	1208.05	12.30	1207.32
0.20	1196.07	12.18	1195.87
0.21	1184.55	11.73	1184.34
3.10	1175.73	11.92	1172.63
		8.39	1167.34
9.57	1184.88	0.42	1175.31
7.70	1190.63	1.95	1182.93
		2.96	1187.67

B.M. set, S. root 24" Maple, L. 17+20

B.M. set, W. Root, Triple Elm., R. 6+10

N.E. Cor. W.H.W., 200' N of S. Hamblen

(1187.78)

B.M. found, Staple, N.E. Root Elm., S.W. of Lam pmaus Co.

2.28	1305.51		1303.23
1.26	1295.56	11.21	1294.30
8.26	1303.65	0.17	1295.39
		1.78	1301.87
1.76	1294.59	10.82	1292.83
7.59	1293.73	8.45	1286.14
		12.60	1281.13
4.74	1298.47	0.00	1293.73
0.02	1286.03	12.46	1286.01
0.33	1273.87	12.49	1273.54
0.93	1262.75	12.05	1261.82
0.15	1250.78	12.12	1250.63
		1.82	1248.96
2.32	1244.83	8.27	1242.51
		1.32	1243.51

N.E. root 15" Maple S.W. cor. {N. Hambden + Old State Rd.

Right, 160+05
B.M. set, W. root, Walnut, Front of Greenwood House

Left, 169+50 Most Northerly of 3
B.M. set, N.E. root, 30" Maple, front of Voladek's House
2' above ground Left, 196+50
B.M. set, Spike, S.E. side 4½' Elm, W. side Rd, in hollow.

~~B.M.~~

Right, 196+45
B.M. set, W. root of S.ly Maple, front of J. Carvers New House

204+75
B.M. set, W. side Twin Cherry, Right

~~0.12~~	0.12 ~~1243.63~~	1243.63		1243.51
	0.92	1232.24	12.31	1231.32
	1.18	1223.70	9.72	1222.52
	1.88	1214.14	11.44	1212.26
			3.31	1210.83
	3.16	1211.41	5.89	1208.25
	3.48	1205.35	9.54	1201.87
	1.30	1195.00	11.65	1193.70
			0.94	1194.06
	8.22	1202.22	1.00	1194.00
	0.12	1190.39	11.95	1190.27
			3.70	1186.69
	0.45	1177.97	12.87	1177.52
	0.18	1170.62	7.53	1170.44
			2.80	1167.82
	0.27	1158.70	12.19	1158.43
T.P.	4.82	1161.13	2.39	1156.31
	0.09	1157.02	4.20	1156.93
			3.14	1153.88

Marks, Gray.
Jan. 8, 1925 Clear, 24°, Snow 12" Deep.

Left, 222+90 500'S. of J. Bryant's House
B.M. set, E. Root, 5" ⌀, Maple of Row on W. Side

Right 236+50 House
B.M. set, W. root, Evergreen, Front of O.A. Shattuck's

Right 247+90 House
B.M. set, W. root Evergreen, Front of S. Side, Maltbie's

Left. 255+85 S. of Road running West
B.M. set, Spike, E side of Hickory, 1' above ground

Spike, W. side Maple, R. of ℄, 200'± N of Culvert

Right, 274+15
B.M. set, W. Root, N. Evergreen Front of Dryer's House

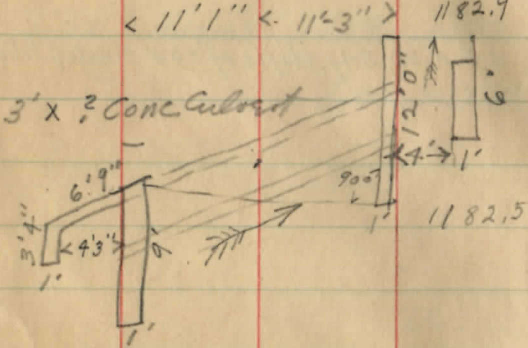
	1157.02		
1.58	1152.64	5.96	1151.06
3.02	1147.01	8.65	1143.99
1.93	1137.56	11.38	1135.63
0.93	1127.59	10.90	1126.66
		9.20	1118.39
0.94	1116.29	12.24	1115.35
1.38	1106.68	10.99	1105.30
		8.38	1098.30

B.M. Set N.E. root 36" Elm, 200' W. of Zikursh's House
Left, 292+20

B.M. Set, S.E. Root, S-ly. Maple of row Front of Johnson's House

	2.37	1190.04		1187.67
0 ~~+30~~			5.0	1185.0
0 - 30			2.8	1187.2
0			5.0	1185.0
0 + 40			5.4	1184.6
1 + 00				1182.9
1 + 72				1182.5
2 + 00			8.4	1181.6
⊼	4.53	1183.87	10.70	1179.34
2 + 50				
3			4.2	1179.7
3 + 20			4.3	1179.6
~~4~~ 4 + 00			9.8	1174.1
4 + 15	Outlet of Lampmans 12" Tile			

3' x ? Conc Culvert



This section not necessary for Earthwork calculation;

Mar. 11, 1925 Marks, Gray, Sprague 7

Staple NE root

B.M. Elm S.W. of Lampman's Cor.

1187.9 — 2.1 / 100

1185.0 — 5.0 / 0   1185.4 — 4.6 / 14   1182.9 — 7.1 / 45   1181.1 — 8.9 / 100

+0.7 4.7/30   -0.1 5.5/21   -1.9 7.3/19-17   -0.2 5.6/13   0.0 5.4/0   +0.2 5.2/8   -0.4 5.8/14   0.0 5.4/15   -0.3 5.7/19   +0.3 5.1/21   +0.2 5.2/30

+2.1 5.0/30   +1.3 5.8/18   -0.6 7.7/12   -1.5 8.6/10-8   -0.1 7.2/6   0.0 7.1/0   -0.3 7.4/12   -0.7 7.8/14-17   -0.3 7.4/18   -0.3 7.4/20   +1.1 6.0/22-30

-2.9 10.4/11.3   -1.6 9.1/11.1   +0.4 7.1/11.1   1182.5 0.0 7.5/0   +0.3 7.2/11.2   -1.7 9.2/11.2   -3.1 10.6/11.3

-0.5 8.9/30   -0.8 9.2/10   -0.3 8.7/6   0.0 8.4/0   -0.5 8.9/10   -2.8 11.2/14-16   -0.3 8.7/17   0.0 8.4/19   -2.0 10.4/30

1178.9 — 5.0 / 14.5

inlet to Lampman's Tile 0

+2.3 1.9/30-24   +1.2 3.0/16   +0.2 4.0/12   0.0 4.2/0   -0.6 4.8/7   -1.8 6.0/11-15   +1.0 3.2/18   +0.5 3.7/30

+3.3 6.5/30   +0.8 9.0/17   0.0 9.8/0   0.0 9.8/3   -3.0 12.8/9+11   20   +4.5 5.3/22-30

1171.4 — 12.5 / 18.5   0

18" Locust

~~6.41~~	6.91	1174.25		1167.34	
[illegible]			3.2	1171.0	~~3.2~~
5+50			3.6	1170.6	~~3.6~~
5+59.8			3.7	1170.5	
5+66.6			10.9	1063.3	
5+73.3					
~~5+75~~			~~3.8~~	~~1170.4~~	
6+00			4.7	1169.5	~~4.7~~
7			4.7	1169.5	4.7
8			3.8	1170.4	~~3.8~~
	7.69	1181.41	0.53	1173.72	
9			9.0	1172.4	~~9.0~~
10			6.0	1175.4	~~6.0~~
	10.22	1191.31	0.32	1181.09	

Feb. 7, 1925 Marks, Grau, Reynolds

Cloudy, Thawing. (Unstable Leveling)

B. M. W. Root Triple Elm, Rt, 6+10

-0.9	-1.4	-1.5	-0.8	0.0	0.0	0.0	-2.4	-2.6	-2.7	-1.5		
4.1	4.6	4.7	4.0	3.2	3.2	3.2	5.6	5.8	5.9	4.7		
30-23	22	13	12	8.0	0	5.0	9	14	22	25 30		
-3.9	-1.9	-3.1	-3.9	-0.6	+0.1	0.0	+0.2	-0.4	-3.4	-3.3	-3.7	-5.1
7.5	5.5	6.7	7.5	4.2	3.5	3.6	3.4	4.0	6.8	6.7	7.1	8.5
30-25	21	18	11	5	4	0	9	12	13	17	22	24-30 Cross
-7.2	-7.2	-1.2	+0.8	+0.2	0.0	+0.3	+0.7	-1.3	-7.3			
10.9	10.9	4.9	2.9	3.5	3.7	3.4	3.0	5.0	11.0			
30	4.0	4.0 4.0	3.0	3.0	0	10.5	10.5-11.5	11.5	11.5-30			
~~-3.8~~	~~-3.8~~	~~0.0~~	~~0.0~~	~~0.0~~	~~-3.4~~	~~-4.1~~	~~-3.9~~					
~~7.4~~	~~7.6~~	~~3.8~~	~~3.8~~	~~3.8~~	~~7.2~~	~~7.9~~	~~7.7~~					
25	12	4	0	11	13	21	25					
-2.7	-2.9	-2.3	-0.1	0.0	-0.2	-2.5	-3.2	-3.0				
7.4	7.6	7.0	4.8	4.7	4.9	7.2	7.9	7.7				
25	12	4	3	0	9	13	21	25				
-1.9	-1.8	-0.4	-0.1	0.0	+0.2	-1.3	-1.5	-1.1				
6.6	6.5	5.1	4.8	4.7	4.5	6.0	6.2	5.8				
25	14	10	6	0	7	10	15	25				
-1.3	-0.9	-0.5	0.0	0.0	-0.4	-1.6	-0.2	-0.8				
5.1	4.7	4.3	3.8	3.8	4.2	5.4	4.0	4.6				
25	20	18	10	8	4	7-9	11	25				
-0.7	-0.3	-0.6	0.0	0.0	-0.3	-1.0	+0.4	+0.8				
9.7	9.3	9.6	9.0	9.0	9.3	10.0	8.6	8.2				
25	12	11	8	0	5	8-10	12	25				
+2.2	+1.7	+0.6	-1.0	-0.2	0.0	+0.2	-1.2	+0.4	+1.3	+1.5		
3.8	4.3	5.4	7.0	6.2	6.0	5.8	7.2	5.6	4.7	4.5		
30	19	9	7	6	0	13	13-14	16	20	30		

		1191.31		
11			11.3	1180.0
12			4.6	1186.7
	10.27	1201.00	0.58	1190.73
13			7.6	1193.4
			5.42	1195.58
	10.87	1206.45		1195.58
14			6.2	1200.3
	10.86	1216.83	0.48	1205.97
15			10.7	1206.1
16			6.3	1210.5
	7.98	1221.83	2.98	1213.85
			2.58	1219.25
	2.58	1221.79		1219.21
17			7.5	1214.3
	11.90	1230.19	3.50	1218.29
18			12.1	1218.1
19			8.9	1221.3

+3.2 +3.1 +1.8 -0.9 0.0 0.0 0.0 -1.0 +3.1 +3.4
8.1 8.2 9.5 12.2 11.3 11.3 11.3 12.3 8.2 7.9
30 19 10 7 5 0 10 14 21 30

+2.6 +2.8 +1.2 -1.4 -0.4 0.0 -0.2 -1.5 +2.3 +2.3
2.0 1.8 3.4 6.0 5.0 4.6 4.8 6.1 2.3 2.3
30 23 12 8 5 0 10 14-15 21 30

+3.0 +2.0 +0.5 -2.1 +0.2 0.0 -0.1 -0.8 +0.5 +2.1 +1.8
4.6 5.6 7.1 9.7 7.4 7.6 7.7 8.4 7.1 5.5 5.8
30 16 12 8-7 4 0 13 14.5 17 23 30

Stone at back side Stake 13+00
Mar, 11, 1925 Marks, Grau, Sprague

+4.0 +2.0 +0.9 -0.9 +0.2 0.0 -0.5 -0.5 -1.6 +0.7 +1.2
2.2 4.2 5.3 7.1 6.0 6.2 6.7 6.7 7.8 5.5 5.0
30 20 13 8-9 5 0 4 13 15-17 20 24-30

+3.5 +2.1 -0.9 0.0 0.0 -0.5 -1.2 +0.3 +1.1 +0.8
7.2 8.6 11.6 10.7 10.7 11.2 11.9 10.4 9.6 9.9
30 17 11-9 6 0 11 13-15 17 20 30

+4.0 +2.5 -0.6 0.0 0.0 -0.1 -1.0 +0.7 +1.1 +0.8
2.3 3.8 6.9 6.3 ~~3.6~~ 6.3 6.4 7.3 5.6 5.2 5.5
30 16 11-10 8 ~~16~~ 0 9 13-14 14 19 30

B.M., Maple Left 17+20 (1219.21)

+3.9 +2.4 -0.4 +0.1 0.0 -0.7 +1.1 -0.1
3.6 5.1 7.8 7.4 7.5 8.2 6.4 7.6
30 15 11-9 7 0 14 16 30

+4.6 +2.3 -0.1 0.0 -0.5 -1.2 +0.1 -0.3
7.5 9.8 12.2 12.1 12.6 13.3 12.0 12.4
30 11 4-3 0 15 18 21 30

+2.7 +1.6 -0.3 0.0 -0.7 +0.4 -0.5
6.2 7.3 9.2 8.9 9.6 8.5 9.4
30 8 5 0 16 19 30

		1230.19		
20			6.4	1223.8
21			2.4	1227.8
	7.40	1237.20	0.39	1229.80
21+70			7.9	1229.3
22			7.7	1229.5
22+20	Present Loose Boulder Pile for Drain 12" Culvert Required		7.7	1229.5
23			5.3	1231.9
	8.99	1244.41	1.78	1235.42
24			5.9	1238.5
+58			3.6	1240.8
25			5.9	1238.5
26			8.6	1235.8

+3.2 +1.8 -0.8 0.0 -0.2 -0.6 +0.6 +1.4 +1.6
3.2 4.6 7.2 6.4 6.6 7.0 5.8 5.0 4.8
30 8 5 0 10 12 14 18 30

+2.4 +1.2 -0.7 +0.1 0.0 -0.4 +1.4 +1.3
0.0 1.2 3.1 2.3 2.4 2.8 1.0 1.1
30 12 9-7 5 0 9 11 30

+1.7 +0.7 -0.3 +0.2 0.0 +0.1 -0.3
6.2 7.2 8.2 7.7 7.9 7.8 8.1
30 11 8 6 0 25 30

-0.4 -0.2 -0.5 +0.4 0.0 +0.3 -1.0 -6.3
8.1 7.9 8.2 7.3 7.7 7.4 8.7 14.0
30 13 12 4 0 8 14 30

+2 8.6 +2 8.5 +2 9.9 +2 9.5 +2 9.8 +2 8.5 +2 3.0
8.6 8.7 7.3 7.7 7.4 8.7 14.2 Ravine
30 12 4 0 8 14 30 to S.E

+2.0 +0.5 -0.9 0.0 0.0 +0.4 +1.9 +2.0
3.3 4.8 6.2 5.3 5.3 4.9 3.4 3.3
30 9 5 0 10 19 24 30

+3.3 +2.3 -0.5 +0.1 0.0
2.6 3.6 6.4 5.8 5.9
30 12 6 3 0

-0.6 +1.5 +1.7
6.5 4.4 4.2
11 13 30

+2.0 +1.4 -0.7 0.0
4.6 2.2 4.3 3.6
30 12 5 0

-0.4 -0.8 +0.6 -0.4
4.0 4.4 3.0 4.0
8 11 12 30

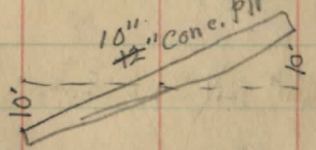
+2.3 +1.9 +1.4 -0.6 0.0 0.0
3.6 4.0 4.5 6.5 5.9 5.9
30 24 9 4 3 0

-0.3 -0.8 -0.4 -0.3 -1.6
6.2 6.7 6.3 6.2 7.5
9 12 14 23 30

+3.7 +1.7 +1.2 -1.0 0.0 0.0
4.9 6.9 7.4 9.6 8.6 8.6
30 14 9 3 1 0

-0.1 -0.8 +0.4 +1.0 -0.7
9.3 9.4 8.2 7.6 8.8
9 12 13 25 30

		1244.41		
	3.32	1236.12	11.61	1232.80
27			5.0	1231.1
28			8.0	1228.1
29			9.8	1226.3
	5.25	1230.59	10.78	1225.34
29+70	No existing Culvert		5.2	
	12" Culvert Required			1225.4
30			5.3	1225.3
31			5.6	1225.0



31+40				
31+56	W. side of N.+S. Rd. 9" Side Road Culvert.			
	Side Road Culvert, 12" E. of ℄ N.+S. Rd.			
31+50			7.7	1222.9

+3.4	+2.4	+1.0	-0.8	0.0	
1.6	2.6	4.0	5.8	5.0	
30	14	6	5-3	0	
-0.5	-0.7	+0.7	+1.8		
5.5	5.7	4.3	3.2		
11	14	15	23	fence	
+2.5	+0.6	-0.8	0.0		
5.5	7.4	8.8	8.0		
30	7	4	0		
-0.3	-0.7	0.0	+0.3		
8.3	8.7	8.0	7.7		
13	16	17	23		
+1.4	-0.4	+0.2	0.0		
8.4	10.2	9.6	9.8		
30	6-4	3	0		
-0.3	-0.7	-0.3	-0.3	+0.3	
10.1	10.5	10.1	10.1	9.5	
10	13	14	17	25	
1125.6	1125.9	1125.2	1125.6	1125.4	
5.0	4.7	5.4	5.0	5.2	
30	9	8-7	6	0	
1125.1		1124.2	1125.0	1123.1	
5.5	6.4	5.6	7.5	Ravine to South	
11	14	15	30		
+0.5	+0.1	-0.6	+0.1	0.0	
4.8	5.2	5.9	5.2	5.3	
30	13	12-10	9	0	
			-0.5	-2.0	
			5.8	7.3	
			12	30	
+3.6	+2.3	-0.1	-1.2	+0.1	0.0
2.0	3.3	5.7	6.8	5.5	5.6
30	23	20	19-18	15	0
		+0.7	-0.1	+0.6	+0.1
		4.9	5.7	5.0	5.5
		8	22	25	30

~~Inadequate~~ Unserviceable

~~Inad~~ Unserviceable

Unserviceable

+2.7	+1.6	0.0	
5.0	6.1	7.7	
30	27	0	
		-0.6	-0.1
		8.3	7.8
		13	30

1230.57

31+73 P.I.			8.0	1222.6
Profile, ℄ of Road South from Corner				
" " " " East " "				
	10.63	1234.61	6.61	1223.98
32			10.6	1224.0
32+50			7.8	1226.8
33			6.1	1228.5
	12.88	1244.30	3.19	1231.42
34			12.1	1232.2
35			8.3	1236.0
36			4.7	1239.6
	7.11	1249.89	1.52	1242.78
37			8.5	1241.4
38			6.8	1243.1
39			5.1	1244.8

8.0

1219.3 1216.1

11.3 14.5

50 100

7.6 (1223.0) 8.3 (1222.3) 10.4 (1220.2)

35 50 100

1223.98

B.M. 2nd tree S. of Cor. on E. side Old St. Rd.

+2.8 +2.6 -1.2 0.0 0.0

5.0 5.2 9.0 7.8 7.8

30 23 14 10 0

-0.5 -1.0 +0.6 +0.5

8.3 8.8 7.2 7.3

10 13-16 20 30

+3.1 +2.2 -1.0 +0.1 0.0

3.0 3.9 7.1 6.0 6.1

30 17 12 7 0

-0.3 -1.5 -0.1 +0.9 +0.9

6.4 7.6 6.2 5.2 5.2

7 11 12 16 30

+3.5 -0.1 -0.2 0.0

7.8 8.6 12.8 12.3 12.1

30 19 12 10 0

-0.2 -1.1 +1.7 +2.8

12.3 13.2 10.4 9.3

7 9-11 15 30

+3.6 +3.4 -1.1 -0.1 0.0

4.7 4.9 9.4 8.4 8.3

30 18 13-11 8 0

0.0 -1.1 +1.6 +2.4

8.3 9.4 6.7 5.9

7 10-12 15 30

+3.0 +2.4 +0.2 -0.8 -0.3 0.0

1.7 2.3 4.5 5.5 5.0 4.7

30 20 13 11 7 0

-1.2 +0.9 +1.1

5.9 3.8 3.6

7-9 12 30

+3.1 +2.1 -0.5 0.0 0.0

5.4 6.4 9.0 8.5 8.5

30 16 12 10 0

-0.5 -1.2 +0.2 +1.1 +1.2

9.0 9.7 8.3 7.4 7.3

4 8 9 15 30

+2.7 +0.3 -0.4 0.0 0.0

4.1 6.5 7.2 6.8 6.8

30 14 13-11 10 0

-0.3 -1.1 +0.4 +0.7

7.3 7.9 6.4 6.1

5 7-9 10 30

+1.9 +0.7 0.0 -1.2 -0.5 0.0

3.2 4.4 5.1 6.3 5.6 5.1

30 21 15 13 10 0

-1.3 +0.1 -0.5

6.4 5.0 5.6

4 10 30

		1249.89		
40			4.1	1245.8
41			2.3	1247.6
	8.31	1257.70	0.50	1249.39
42			9.6	1248.1
43			8.3	1249.4
44			6.1	1251.6
45			4.3	1253.4
46			2.7	1255.0
	8.11	1264.07	1.74	1255.96
47			7.8	1256.3
48			6.3	1257.8
49			5.1	1259.0

+2.7 +0.4 +0.1 -1.3 -0.4 0.0
1.9 3.7 4.0 5.4 4.5 4.1
30 24 14 13-12 11 0

-0.6 -1.2 +0.3 -0.9
4.7 5.3 3.8 5.0
5 7-9 10 30

+0.3 -0.1 0.0 -1.0 -0.1 0.0
2.0 2.4 2.3 3.3 2.4 2.3
30 28 15 14 11 0

-0.6 -1.1 +0.1 -0.8
2.9 3.4 2.2 3.1
7 9 10 30

B.M. Maple Left Sta. 41+60 1249.44

+1.0 +0.2 -0.8 -0.1 0.0
8.6 9.2 9.4 9.7 9.6
30 14 13 10 6

0.0 -0.4 +0.2 +0.3 +0.9
9.6 10.0 9.4 9.3 8.7
4 7-10 11 21 30

+0.7 +0.2 -1.2 -0.6 0.0
7.6 8.1 9.5 8.9 8.3
30 15 13 11 0

-0.3 -1.0 0.0 -0.6 -0.9
8.6 9.3 8.3 7.7 7.4
6 9 10 14 30

+1.0 +0.5 -0.7 -1.5 -0.6 0.0
5.1 5.6 6.3 7.6 6.7 6.1
30 22 19-16 14 10 0

-0.6 -1.5 +0.4 +0.8
6.7 7.6 5.7 5.3
6 9 14 30

+1.8 +1.1 -0.2 -1.6 -0.4 0.0
2.5 3.2 4.5 5.9 4.7 4.3
30 21 17-16 14 10 0

-0.5 -1.4 +0.3 +0.5
4.8 5.7 4.0 3.8
7 10 12 30

+1.3 +1.6 +0.2 -0.7 -1.2 -0.5 0.0
1.4 1.1 2.5 2.9 3.9 3.2 2.7
30 23 18 14 13 10 0

-0.4 -0.8 +0.7 +1.1
3.1 3.5 2.0 1.6
9 12 14 30

+0.5 +1.0 -0.2 -1.1 -0.3 0.0
7.3 6.8 8.0 8.9 8.1 7.8
30 23 15 13 9 0

-0.3 -0.8 +0.3 +0.4
8.1 8.6 7.5 7.4
8 11 12 30

-0.4 -0.7 -1.2 -0.5 0.0
6.7 6.5 7.5 6.8 6.3
30 23 12 9 0

-0.3 -0.7 -0.2 -1.0
6.6 7.0 6.5 7.3
7 9 10 30

-0.5 0.0 -0.3 -0.8 -0.3 0.0
5.6 5.1 5.4 5.9 5.4 5.1
30 22 14 12-11 10 0

-0.3 -0.7 -0.3 -1.3
5.4 5.8 5.4 6.4
6 8-9 10 16-30

		1264.07		
50			4.2	1259.9
51			3.0	1261.1
52			1.4	1262.7
	9.29	1272.93	0.43	1263.64
53			8.7	1264.2
54			7.2	1265.7
55			5.4	1267.5
56			3.8	1269.1
57			2.0	1270.9
	11.21	1283.87	0.27	1272.66
58			10.9	1273.0
59			8.7	1275.2

+0.1	-0.1	-0.7	-0.2	0.0		
4.1	4.0	4.9	4.4	4.2		
30	14	13	10	0		
+0.5	+0.7	-0.1	-0.3	-0.9	-0.3	0.0
2.5	2.3	3.1	3.3	3.9	3.5	3.0
30	21	19	15	14	11	0
+1.7	+1.7	-0.7	-1.3	-0.5	0.0	
0.4	0.4	2.1	2.7	1.9	1.4	
30	21	14	13	10	0	
+1.3	+1.5	-0.2	-1.3	-0.5	0.0	
7.4	7.2	8.9	10.0	9.2	8.7	
30	20	13	11	9	0	
+1.2	+1.4	-0.1	-1.0	-0.5	0.0	
6.0	5.8	7.3	8.2	7.7	7.2	
30	20	13	12	10	0	
+1.1	+1.3	-0.3	-1.2	-0.6	0.0	
4.3	4.1	5.7	6.6	6.0	5.4	
30	19	12	11	10	0	
+1.1	+1.3	-0.2	-1.0	-0.3	0.0	
2.7	2.5	4.0	4.8	4.1	3.8	
30	19	14	12	10	0	
+0.8	+0.9	+0.2	-0.7	-0.2	0.0	
1.2	1.1	1.8	2.7	2.2	2.0	
30	20	14	13	10	0	
+0.4	+0.8	+0.2	-1.0	-0.5	0.0	
10.5	10.1	10.7	11.9	11.4	10.9	
30	21	13	12	10	0	
+2.0	+1.8	0.0	-0.6	-0.2	0.0	
6.7	6.9	8.7	9.3	8.9	8.7	
30	26	14	13	10	0	

+0.2	-0.5	0.0	-1.0	-0.7		
4.0	4.7	4.2	5.2	4.9		
6	7-8	9	20	30		
-0.1	-0.7	0.0	+0.1	+0.2	+0.3	
3.1	3.7	3.0	2.9	3.2	2.7	
5	9	10	19	21	30	
-0.6	-1.2	-0.2	+0.4			
2.0	2.6	1.6	0.8			
6	9	10	30			
-0.3	-1.2	-0.5	+0.2	+0.4		
9.0	9.9	9.2	8.5	8.3		
7	7	10	17	30		
-0.3	-0.8	0.0	0.0			
7.5	8.3	7.2	7.2			
7	10	11	30			
-0.3	-1.0	-0.1	+0.3			
5.7	6.4	5.5	5.1			
8	11	12	30			
-0.3	-0.9	+0.1	+0.3			
4.1	4.7	3.7	3.5			
7	9	11	30			
-0.2	-0.8	0.0	+0.3			
2.2	2.8	2.0	1.7			
6	9	10	30			
-0.4	-0.8	+0.2	+0.1			
11.3	11.7	10.7	10.8			
7	9	10	30			
-0.1	-0.8	+0.2	+1.6	+1.4		
8.8	9.5	8.5	7.1	7.3		
7	11	12	25	30		

		1283.87		
60			6.2	1277.7
61			3.5	1280.4
			0.82	1283.05
	12.95	1296.06		1283.11
62			13.1	1283.0
63			10.2	1285.9
64			6.5	1289.6
	12.44	1306.31	2.19	1293.87
65			13.0	1293.3
66			10.3	1296.0
67			6.9	1299.4
68			4.9	1301.4

+2.0	+1.9	+0.2	-0.6	-0.3	0.0		-0.4	-0.3	+1.0	+1.6		
4.2	4.3	6.0	6.8	6.5	6.2		6.6	6.5	5.2	4.6		
30	24	16	14	10	0		11	15	22	30		
+1.1	+0.9	-0.8	-0.5	0.0			-0.1	-1.1	-0.6	+1.2	+0.9	
2.4	2.6	4.3	4.0	3.5			3.6	4.6	4.1	2.3	2.6	
30	17	13	8	0			8	10	16	20	30	

B.M. Maple, Rt. 61+30 (1283.11)

Mar. 13, 1925, Cloudy, Marks, Gray, Sprague

+2.7	+1.2	+0.4	0.0				-0.2	-0.7	+0.1	+1.1		
10.4	11.9	12.7	13.1				13.3	13.8	13.0	12.0		
30	12	10	0				7	12	17	30		
+1.8	+1.3	+0.2	-0.4	-0.1	0.0		-0.4	-0.6	+0.1	+0.5	+2.4	+1.5	+1.5
8.4	8.9	10.0	10.6	10.3	10.2		10.6	10.8	10.1	9.7	7.8	8.7	8.7
22.5	17	15	12	10	0		6	9	11	14	17	24	30
Fence													
+2.3	+2.3	0.0	-0.7	0.0	0.0		-0.1	-0.5	+2.1	+1.4	+1.4	
4.2	4.2	6.5	7.2	6.5	6.5		6.6	7.0	4.4	5.1	5.1	
24	18	14	13	12	10	0	5	7	11	23	30	
Fence												
+3.0	+2.6	-0.8	-0.3	0.0			-0.3	-1.1	-0.1	+1.6	+1.1	+1.1
10.0	10.4	13.8	13.3	13.0			13.3	14.1	13.1	11.4	11.9	11.9
25	20	12	9	0			10	12	13-16	20	24	30
Fence												
+4.1	+4.1	-0.6	-0.1	0.0			-0.1	-1.1	+2.8	+3.0		
6.2	6.2	11.1	10.4	10.3			10.4	11.4	7.5	7.3		
30	21	12	9	0			9	13	21	30		
+2.2	+2.1	+1.2	-0.3	0.0			-0.5	-1.4	+0.8	+1.5	+1.6	
4.7	4.8	8.1	7.2	6.9			7.4	8.3	6.1	5.4	5.3	
30	27	14	11	0			9	12	17	21	30	
+1.6	+1.1	-0.1	-1.1	-0.5	0.0		-0.3	-1.0	+0.1	+1.1	+1.3	
3.3	3.8	5.0	6.0	5.4	4.9		5.1	5.9	4.8	3.8	3.6	
30	18	14	13	7	0		8	12	13	20	30	

		H.I.		
	Back Sight	1306.31	F.S.	E.I.
69			3.3	1303.0
	11.06	1313.93	3.44	1302.87
70			9.3	1304.6
71			7.6	1306.3
72			5.9	1308.0
73			4.4	1309.5
74			3.7	1310.2
75			3.5	1310.4
	4.04	1314.36	3.61	1310.32
76			4.2	1310.2
77			4.9	1309.5

Left

+1.8	+0.8	-1.0	-0.4	0.0
1.5	2.5	4.3	3.7	3.3
30-28	19	14	12	0
+1.7	-1.2	-1.0	-0.3	0.0
7.6	10.5	10.3	9.6	9.3
30-26	21	15	12	0
+1.3	-0.2	-1.1	-0.4	0.0
6.3	7.8	8.7	8.0	7.6
30-27	15	13	10	0
+0.2	+0.8	-0.2	-1.1	-0.5	0.0
5.7	5.1	6.1	7.0	6.4	5.9
30	23	12	11	8	0
+0.5	+0.1	-0.9	-0.2	0.0
3.9	4.3	5.3	4.6	4.4
30	13	12	9	0
-0.4	+0.1	-0.9	-0.9	-0.4	0.0
4.1	3.6	4.1	4.6	4.1	3.7
30	25	14	12	10	0
-0.6	-0.4	-0.9	-0.2	0.0
4.1	3.9	4.4	3.7	3.5
30	15	13	8	0
-0.3	+0.7	-0.6	0.0	-0.8	-0.4	0.0
4.5	4.0	4.8	4.2	5.0	4.6	4.2
30	25	18	14	12	10	0
+0.2	+0.4	-0.2	-1.1	-0.7	0.0
4.7	4.5	5.1	6.0	5.6	4.9
30	23	12	11	8	0

Right (EAST)

-0.2	-0.7	+0.1	+0.6
3.5	4.0	3.2	2.7
8	11	13	30
-0.1	-0.6	+0.6	+1.4
9.4	9.9	8.7	7.8
7	11	13	30
-0.2	-0.7	+0.5	+0.9
7.8	8.3	7.1	6.7
8	11	14	30
0.0	-0.6	+1.0	+1.5
5.9	6.5	4.9	4.4
11	18	21	30
-0.1	-0.8	+0.8	+1.1
4.5	5.2	3.6	3.3
9	13	16	30
-0.4	-1.3	-0.2	+0.9
4.1	5.0	3.9	2.8
8	12	14	30
-0.3	-0.9	+0.4	+0.8	+1.5
3.8	4.4	3.1	2.7	2.0
7	10	14	17	30
-0.1	-0.8	+1.1	+1.7
4.3	5.0	3.1	2.5
8	12	15	30
-0.2	-0.7	+0.8	+1.6
5.1	5.6	4.1	3.3
8	12	16	30

		1314.36		
78			6.6	1307.8
79			8.4	1306.0
80			11.1	1303.3
			5.39	1308.97
	5.39	1314.46		1309.07
		1306.67		
	3.68	~~1313.67~~	11.47	1302.99
81			7.8	1298.9
82			12.7	1294.0
		1296.68		1294.04
	2.64	~~1293.68~~	12.63	~~1291.04~~
83			6.2	1290.5
84			9.0	1287.7
85			11.5	1285.2
		1287.79		1285.08
	2.79	~~1284.11~~	11.68	~~1282.00~~
86			4.7	1283.1

17

+0.9 +0.3 +1.1 +1.0 -0.9 -0.4 0.0
5.7 6.3 5.5 5.6 7.5 7.0 6.6
30 25 20 14 9 8 6

-0.1 +0.5 +2.5
6.7 6.1 4.1
11 14 30

+0.1 +0.7 +1.1 +1.2 +0.1 -0.8 -0.4 0.0
8.3 7.7 7.3 7.2 8.3 9.2 8.6 8.4
30 ~~20~~ 19 15 10 9 6 0

0.0 -0.2 +0.5 +1.5 +2.9
2.4 8.6 7.9 6.9 5.5
9 12 13 16 30

+2.4 +0.1 -0.9 -0.1 0.0
8.7 11.0 12.0 11.2 11.1
24 16 14 11 0

-0.4 -0.9 +2.4 +4.5
11.5 12.0 8.7 6.6
4 9 10 30

B.M. Elm. R. 79+75 (1309.07)

+1.9 +2.2 -1.8 -1.0 0.0
5.9 5.6 9.6 8.8 7.8
30 26 15 13 0

-0.2 -0.7 +3.1 +3.6 +4.4
8.0 8.5 4.7 4.2 3.4
4 5 16 22 30

+1.7 +2.3 -1.4 -0.3 0.0 -0.1 -0.5 +0.4 +1.8 +2.6 +3.7
11.0 10.4 14.1 13.0 12.7 12.8 13.2 12.3 10.9 10.1 9.0
30 26 15 12 0 4 7 8 14 22 23-30

+1.2 +1.7 +0.6 -1.3 -0.4 0.0 -0.3
5.0 4.5 5.6 7.5 6.6 6.2 6.5
30 26 17 14-13 11 0 7

-1.5 +1.1 +2.2 +3.2 +3.5
7.7 5.1 4.0 3.0 2.7
12 15 24 26 30

+0.8 +0.5 +1.2 +0.3 -1.5 -0.6 0.0
8.2 8.5 7.8 8.7 10.5 9.6 9.0
30 26 23 13 12 8 8

-0.4 -1.2 +0.7 +1.3 +2.3
9.4 10.2 8.3 7.7 6.7
8 13 17 26 30

+0.5 +1.0 0.0 -1.1 -0.3 0.0
11.0 10.5 11.5 12.6 11.8 11.5
30 20 12 11 7 0

-0.4 -1.0 0.0 +0.9 +2.6
11.9 12.5 11.5 10.6 9.9
9 14 16 18 30

+0.5 +0.4 -1.3 -0.3 0.0
4.2 4.3 6.0 5.0 4.7
30-16 10 8 6 0

-0.2 -0.6 -0.3 +0.2
4.9 5.3 5.0 4.0
11 14 16 30

= Fence

		1287.79 ~~1284.79~~		
87			6.4	1281.4
88			7.9	1279.9
	1.71	1279.96 ~~1276.96~~	9.54	1278.25 ~~1275.25~~
89			2.0	1278.0
90			5.1	1274.9
~~91~~				
91			11.7	1268.3
	1.85	1269.21 ~~1266.21~~	12.60	1267.36 ~~1264.36~~
91+65			2.6	1266.6
			2.9	1266.3
91+82	2½ x 3' Stone Culvert Unserviceable			
	New Culvert Required ~~at~~ on skew			
	Outlet at Sta 91+90			
	Inlet " 91+75			
92			2.8	1266.4
			3.56	1265.65 ~~1262.65~~

0.0 +0.5 +0.5 -0.9 -0.2 0.0 +0.2 -0.4 +0.4 +0.3

6.4 5.9 5.9 7.3 6.6 6.4 6.2 6.8 6.0 6.1

30 16 9 7 4 0 10 14 15 30

Fence

+0.3 +0.6 +0.8 -0.9 -0.5 0.0 +0.1 -0.7 +0.6 +0.2

7.6 7.3 7.1 8.7 8.4 7.9 7.8 8.6 7.3 7.7

30 16 9 8 6 0 10 13 15 30

Fence

+1.5 +0.4 -0.9 -0.4 0.0 +0.1 -1.4 +0.7 +1.6 +1.4

0.5 ~~1.6~~ 2.9 2.4 2.0 1.9 3.4 1.8 0.4 0.6

30 19 16 10 7 6 0 11 14 16 22 30

Fence

+3.2 +3.0 +1.0 +0.8 -1.1 -0.4 0.0 0.0 -2.1 -0.1 +3.4

1.9 2.1 4.1 4.3 6.2 5.5 5.1 5.1 7.2 5.2 1.7

30 21 15 10 8 7 0 11 14 16 28 30

+7.3 +1.1 -0.3 -1.1 -0.4 0.0 -0.2 -0.8 +0.3 +1.0 +5.1

4.4 10.6 12.0 12.8 12.1 11.7 11.9 12.5 11.4 10.7 6.6

40 35 21 18 15 12 11 7 0 11 12 15 19 30

-2.5 -2.7 -1.9 -0.2 0.0 -0.3 -1.3 -1.7 -2.9

5.1 5.3 4.5 2.8 2.6 2.9 3.9 4.3 5.5

30 17 16 10 0 7 10 19 30

1255.7 1257.7 1260.6 1264.9 1264.6 1266.3 1266.3 1266.4 1265.0 1265.2 1261.7 1258.7 1261.8

3.5 11.5 8.6 4.3 4.2 2.7 2.9 2.8 4.2 4.0 7.5 10.5 7.3

30 15 14.8 13.8 13 8 0 6 10 11.5 12.5 12.5 12.6 34

+28

Top of ledge rock

-11.2 0.0 0.0 -0.1 -2.3 -3.8 -2.8

14.0 2.8 2.8 2.9 5.1 6.6 5.6

30 25 9 0 8 14 23 30

(1265.63) B.M. Maple left of ~~92+20~~ 93+20

Stakes are to be corrected by adding 100 feet to original marking.

	7.95	1273.58		1265.63
93			6.2	1267.4
93+30			5.7	1267.9
94			8.9	1264.7
95			12.4	1261.2
	6.05	1266.97	12.66	1260.92
			7.4	1259.6
95+95	12"X12" Plank Sluice Requires 15" Pipe			Use section for culvert design only
96			7.3	1259.7
97			5.9	1261.1
	7.69	1272.99	1.67	1265.30
98			5.7	1267.3
+60			4.2	1268.8
99			4.7	1268.3
100			6.3	1266.7
101			7.9	1265.1

Mar. 16, 1925 Marks, Gray, Sprague 19
Fair.

B.M. Maple Left 93+20

-1.8 0.0 -0.4 0.0 +0.2 +2.7 +5.2
8.0 6.2 6.6 6.2 6.0 3.5 1.0
30 16 12 0 12 25 30

+0.6 0.0 -0.6 -0.2 0.0 -0.2 -0.7 +1.3 +3.2 +5.2
8.3 8.9 9.5 9.1 8.9 9.1 9.6 7.6 5.7 3.7
30 13 12 10 0 6 8 13 21 28-30

+0.6 +0.8 -0.5 -1.2 -0.8 0.0 -1.1 -0.6 -0.6 +3.1 +3.6
11.8 11.6 12.9 13.6 13.2 12.4 13.5 13.0 13.0 9.3 8.8
30 21 18-14 12 9 0 10 11 18 27 30

12.52.00 12.56.8 12.59.2 12.59.6 12.59.3 12.56.5 12.57.6
13.0 10.2 10.2 7.8 7.4 7.7 10.5 9.4
100 30 9 8 0 8 8.5 F.L. 30

-2.6 -1.4 -1.7 -0.2 0.0 -0.4 -1.2 -2.1
9.9 8.7 9.0 7.5 7.3 7.7 8.5 9.4
30 14 11 8 0 8 11 30

+1.9 +2.3 +0.2 -0.9 -0.3 0.0 -0.2 -1.2 +0.1 +2.1 +3.6
4.0 3.6 5.7 6.8 6.2 5.9 6.1 7.1 5.7 3.8 2.3
30 25 14 14 10 0 5 8 9 15 30

+0.5 +0.2 -1.3 -0.5 0.0 -0.4 -0.9 +1.1 +3.2
5.2 5.5 7.0 6.2 5.7 6.1 6.6 4.6 2.5
27 15 13 9 0 7 8 11 30
fence

+0.3 +0.3 -1.3 -0.7 0.0 -0.9 -0.1 +1.2
4.4 4.4 6.0 5.4 4.7 5.6 4.8 3.5
27 14 10 8 0 10 11 30
fence

-1.2 -0.4 -1.0 -0.5 0.0 -0.3 -0.8 -0.3 +0.8
7.5 6.7 7.9 6.8 6.3 6.6 7.1 6.6 5.5
28 12 11 9 0 7 9 11 30
fence

+0.3 +0.1 -1.4 -0.5 0.0 -0.4 -1.1 +1.2 +3.6
7.6 7.8 9.3 8.4 7.9 8.3 9.0 6.7 4.3
26 13 10 8 0 7 9 13 30
fence

		1272.89		
102			11.1	1261.9
	1.33	1263.25	11.07	1261.92
103			4.9	1258.4
104			8.7	1254.6
105			11.4	1251.9
	6.38	1257.82	11.81	1251.44
106			6.2	1251.6
106+35	3' Stone Culvert		6.4	1251.4
	Requires 3' x 3' Ext. on Left.			
107			7.2	1250.6
B.M. 107 +75	20" Hemlock		0.77	1257.05
108			5.4	1252.4
109			5.1	1252.7

+0.6 +0.8 +0.9 -1.0 -0.4 0.0 -0.1 -0.7 +0.6 +1.3
10.5 10.3 10.2 12.1 11.5 11.1 11.2 11.8 10.5 8.8
30 24 11 9 7 0 9 12 14 30
fence

+1.7 +1.1 -1.3 -0.5 0.0 -0.2 -0.9 +0.8 +2.3 +3.4
3.2 3.8 6.2 5.4 4.9 5.1 5.8 4.1 2.6 1.5
24 11 7 5 0 10 13 15 21 30

+1.7 +1.7 +1.0 +0.1 -0.9 -0.2 0.0 -0.3 -1.4 +0.1 +2.0 +3.6
7.0 9.0 7.7 8.6 9.6 8.9 8.7 9.0 10.1 8.6 6.7 5.1
25 17 10 8 7 4 0 9 11 14 21 30

+1.1 -0.1 -0.5 0.0 +0.4 +0.11 -0.7 -0.5 +0.2 +2.0
10.3 11.5 11.9 11.4 11.0 11.3 12.1 11.9 11.2 9.4
25 9 8 8 4 9 11 15 16 30

-2.4 -0.9 -1.4 -0.8 0.0 -0.7 -1.6 -1.0 -1.3
8.6 7.1 7.6 7.0 6.2 6.9 7.8 7.2 7.5
27-30 11 9 7 0 11 13-15 10 30

+2.46 +2.48.5 +2.86 +2.49.5 +2.51.8 +2.51.1 +2.51.4 +2.51.2 +2.51.8 +2.49.4 +2.48.4 +2.49.6
11.2 9.3 9.2 8.3 6.0 6.7 6.4 6.6 6.0 8.4 9.4 8.2
30 8.3 8.3 8.3 7 0 11 12.5 12.5 12.5 30

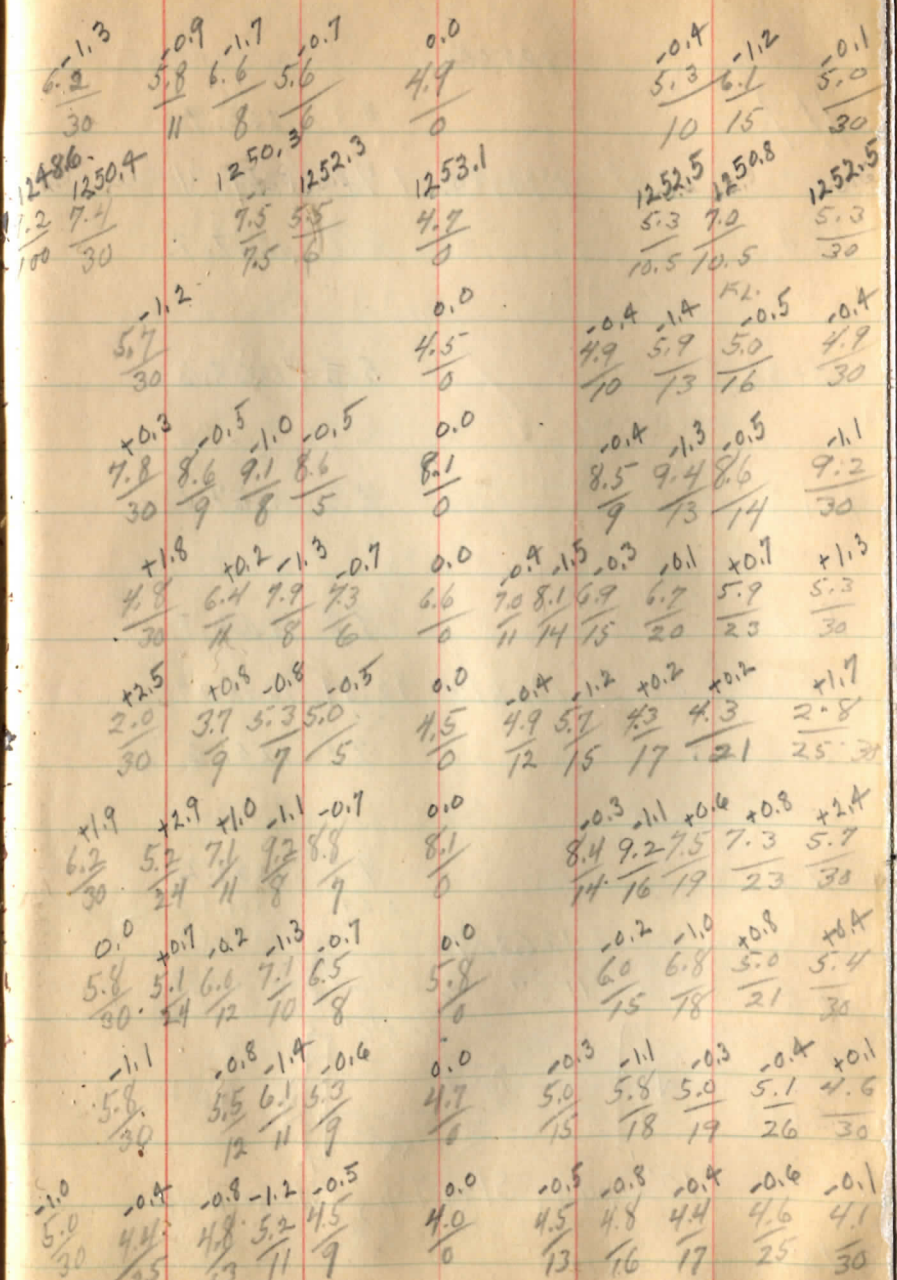
-0.8 -0.3 -0.8 -0.3 0.0 -0.2 -0.8 -0.8 +0.5
8.0 7.5 8.0 4.5 7.2 7.4 8.0 8.0 6.7
26 13 11 9 0 9 12 17 29

1257.08 +0.1 +0.5 -1.9 -0.3 0.0 +0.1 +1.6 +3.8
5.3 4.9 7.3 5.9 5.4 5.3 3.8 1.6
30 15 11 8 0 10 12 30

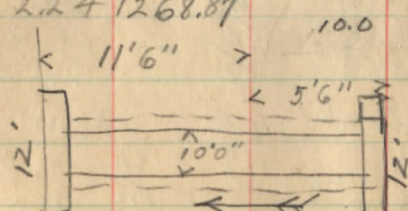
-0.7 -0.4 -1.2 -0.5 0.0 -0.3 -1.2 -0.5 +1.1
5.8 5.5 6.3 5.6 5.1 5.4 6.3 5.6 4.0
30 11 8 5 0 12 15 17 30

1257.82

110			4.9	1252.9
110+15	10" Vitrified Pipe		4.7	1253.1
	15" Pipe Required			
111			4.5	1253.3
	7.95	1262.73	3.04	1254.78
112			8.1	1254.6
113			6.6	1256.1
114			4.5	1258.2
	7.27	1269.02	0.98	1261.75
115			8.1	1260.9
116			5.8	1263.2
117			4.7	1264.3
118			4.0	1265.0



		1269.02		
119			3.1	1265.9
	7.09	1274.40	1.71	1267.31
120			6.7	1267.7
120+35			5.8	1268.6
121			7.3	1267.1
122			9.7	1264.7
	6.71	1268.70	12.31	1262.09
123			7.1	1261.6
124			9.5	1259.2
			2.24	1266.46
	2.24	1268.87		1266.63
			10.0	
125				1258.9
125+45				1260.4



10' Span, Slab Top, Stone Walls
Requires Extension

126		
	8.4	1260.5

0.0 +0.7 +0.3 -0.8 -0.3 0.0
3.1 2.4 2.8 3.9 3.4 3.1
30 25 15 13 7 0

-0.6 0.0 +0.1 +1.6
3.7 3.1 3.0 1.5
15 16 24 30

+0.9 +0.1 0.0
5.8 6.6 6.7
30 15 0

+0.4 +1.4
6.3 5.3
14 30

+0.6 0.0 0.0
5.2 5.8 5.8
30 13 0

+0.7 +1.2 +3.4
5.1 4.6 2.7
18 20 30

+0.3 0.0 -1.0 -0.8 0.0
7.5 7.3 8.3 8.1 7.3
30 23 17 15 0

+0.3 -0.3 +0.3 +1.7 +3.7
7.0 7.6 7.0 5.6 3.6
10 11 12 20 30

+0.7 +0.2 -0.1 -1.6 -0.5 0.0 0.0
9.0 9.5 9.8 11.3 10.2 9.7 9.7
30 26 20 17 14 10 0

-0.4 -1.0 +0.6 +1.1 +1.3
10.1 10.7 7.1 8.6 8.4
4 8 10 25 30

+2.6 -0.7 -1.8 -1.1 -0.3 0.0
4.5 7.8 6.9 8.2 7.4 7.1
30 17 15 13 8 0

-0.5 -1.5 +0.1 +0.7 +2.9
7.6 8.6 7.0 6.4 4.2
4 8 11 24 30

-1.3 -0.9 -0.8 -0.6 -0.1 0.0
10.8 9.9 10.3 10.1 9.6 9.5
30 16 15 12 7 0

-0.4 -1.2 -0.6 -1.1 +0.5
9.9 10.7 10.1 10.6 9.0
5 9 10 16 30

B.M. 1271.55

-1.6 -0.8 -1.6 -0.2 0.0
11.6 10.8 11.6 10.2 10.0
30 17 15 11 0

-0.3 -1.0 -2.0 -1.4 -1.9
10.3 11.0 12.0 11.4 11.9
5 10 15 17 30

1254.9 1255.4 1259.2 1261.2 1260.8 1260.4 1260.8 1261.3 1259.3 1255.7 1256.4
14.0 13.5 9.7 7.7 8.1 8.5 8.8 7.6 9.6 13.2 12.3
30 11.5 11.5 11.5 10.5 0 4.5 5.5 5.5 5.5 30

-1.9 -1.5 -0.4 -1.8 -0.8 -0.2 0.0
10.3 9.9 8.8 10.2 9.2 8.6 8.4
30 25 19 17 13 9 0

-1.0 -2.0 -1.0 -1.8
9.4 10.4 9.4 10.2
6 11-8 12 30

		~~1268.70~~ 1268.87				
127			7.5	1261.4	+0.7 6.8/30, +0.1 7.4/17, -0.8 8.3/16, -0.4 7.9/14, -0.2 7.7/8, 0.0 7.5/0	-0.4 7.9/4, -1.3 8.8/8, -0.5 8.0/11, -0.5 8.0/18, +1.1 6.4/25, +1.4 6.1/30
	10.43	1277.36		1266.63		
128			13.3	1264.1	+5.0 8.3/30, +2.7 10.6/23, -0.9 14.2/18, -0.2 13.5/15, 0.0 13.3/0	-0.3 13.6/4, -1.3 14.6/7, -0.6 13.9/8, +4.2 9.1/18, +5.8 7.5/27, +5.8 7.5/30
129			8.5	1268.9	+2.5 6.0/30, +2.3 6.2/24, +1.5 7.0/21, -1.0 9.5/18, -0.1 8.6/16, +0.1 8.4/7, 0.0 8.5/0	-0.5 9.0/4, -1.2 9.7/6, -1.7 10.2/8, +1.8 6.7/15, +3.8 4.7/27
	12.55	1288.08	1.83	1275.53		
130			15.0	1273.1	+2.9 12.1/30, +2.0 13.0/23, -1.0 16.0/17, -0.4 15.4/15, 0.0 15.0/0	-0.4 15.4/5, -1.3 16.3/7, +3.0 12.0/19, +4.3 10.7/30
131			10.7	1277.4	+7.0 3.7/30, +6.3 4.4/24, -0.6 11.3/13, +0.1 10.6/11, 0.0 10.7/0	0.0 10.7/7, -1.1 11.8/10, +1.0 9.7/12, +2.3 8.4/17, +2.1 8.6/30
132			5.4	1282.7	+3.4 2.0/30, +0.7 4.7/15, -0.7 6.1/14, 0.0 5.4/11, 0.0 5.4/0	0.0 5.4/6, -1.2 6.6/9, +0.6 4.8/13-18, +2.5 2.9/25, +2.3 3.1/30
	8.56	1296.34	0.30	~~1287.78~~ 1287.78		
133			9.4	1286.9	+2.0 7.4/30, +1.4 8.0/17, -1.7 11.1/12, -0.7 10.1/10, 0.0 9.4/0	-0.7 10.1/10, -1.6 11.0/13, +3.6 5.8/25-30
134			6.6	1289.7	+0.4 6.2/30, 0.0 6.6/17, -1.7 8.3/15, -0.8 7.4/12, 0.0 6.6/0	-0.3 6.9/12, -1.3 7.9/15, +1.9 4.7/22, +2.3 4.3/30
135			5.3	1291.0	-1.1 6.4/30, -0.5 5.8/18, -1.4 6.7/16, -0.9 6.2/13, 0.0 5.3/0	+0.4 4.9/13, -0.9 6.2/16, +0.1 5.4/17, +0.7 4.6/30
B.M. Rt. 135+50			3.33	1293.01	(1293.05)	

	3.33	1296.38		1293.05
136			4.3	1292.1
	9.06	1303.30	2.14	1294.24
137			8.2	1295.1
138			6.7	1296.6
138+50			5.4	1297.9
139			6.6	1296.7
140			7.2	1296.1
141			8.0	1295.3
			6.7	1296.6
141+60	3'X6' Cover Slab Broken Stone Culvert 2½X2½ No floor			
	10.50	1306.70	7.10	1296.2
142			10.6	1296.1
143			9.7	1297.0
144			7.6	1299.1

+0.8 -0.3 -0.4 -1.5 -0.8 0.0
3.5 4.6 4.7 5.8 5.1 4.3
30 24 15 13 9 0

-0.8 -1.1 -0.6
5.1 5.4 4.9
10 13 15-30

+1.0 +0.8 -1.3 -0.7 0.0
7.2 7.4 9.5 8.9 8.2
30 17 11 8 0

-0.6 -2.0 +3.0 +3.4
8.8 10.2 5.1 4.8
9 15 24 30

+0.8 +0.3 -0.7 -0.2 +0.2 0.0
5.9 6.4 7.4 6.9 6.5 6.7
30 19 16 14 6 0

-0.1 -0.6 +2.3 +3.2
6.8 7.3 4.4 3.5
7 10 19 30

-0.2 -0.6 -1.8 -1.1 0.0 0.0
6.8 7.2 8.4 7.7 5.4 6.6
28 24 22 16 5 0
Side Walk

-1.4 +1.2 +2.0
8.0 5.4 4.6
10 17 28 Fence

-1.1 -1.3 -2.3 -0.7 0.0
8.3 8.5 9.5 7.9 7.2
27 21 18 9 0
S.W.

-0.6 -1.6 -0.1
7.8 8.8 7.3
4 9 30

-0.8 -1.0 -1.8 -0.8 0.0
8.8 9.0 9.8 8.8 8.0
27 19 16 10 0
S.W

-0.4 -1.4 +0.7
8.4 9.4 7.3
6 12 30

1293.0

-.5 -1.1
12.5 10.7 10.3 8.1 5.5 7.1 6.7 7.0 5.5 8.1 10.4 10.2
100 30 12.5 12.5 12.5 10.5 9 0 9 11.2-12.5 12.5 12.5 30

-1.9 -1.8 -2.4 -1.0 0.0
12.5 12.4 13.0 11.6 10.6
26 17 15 11 0
S.W

-0.9 -2.3 -1.6 -1.3
11.5 12.9 12.2 11.9
10 14 18 30

-1.1 -1.3 -1.7 -0.6 0.0 -0.8 -1.9 -0.7 -0.3
10.8 11.0 11.4 10.3 9.7 10.5 11.6 10.4 10.0
25 19 14 7 0 13 16 18 30
S.W

+0.5 -0.3 -2.1 -0.8 0.0
7.1 7.9 9.7 8.4 7.6
24 20 16 10 0
S.W

-1.1 -1.9 +0.1 +1.4
8.7 9.5 7.5 6.2
11 13 17 30

	1306.70		
145		4.0	1302.7
	S. Edge Conc. Pav.		
145+28		1.2	1305.5
	N. Edge Conc. Pav.		
145+39		1.1	1305.6
		3.45	1303.25

+0.5 -0.3 0.0

3.5 4.3 4.0

34 17 0

S.W.

-0.3 -1.4 +0.4 +1.1

4.3 5.4 3.6 2.9

6 11 15 30

-1.5 0.0 +1.2

2.6 1.1 +0.1

100 0 50

1303.23

B.M. Maple, S.W. cor. Old St. Rd. + N. Hamb. St.

Mar 25, 1925 Marks, Gray, Sprague
Cloudy

B.M. S.W. Cor. Old State Rd + N. Hampden St

	1.77	1303.00		1303.23	
146				1301.7	
147				1301.2	
148				1300.8	
149				1300.1	
150				1299.1	
	1.33	1300.78	5.55	1299.45	
150+49	10" Conc. Pipe, Fair Condition			1298.7	
151				1297.4	
152				1293.7	
153				1289.8	

		-0.6	-0.5	+0.1	0.0			0.0	-0.6	+1.3	+1.5
		3.9	3.8	3.2	3.3			3.3	3.9	2.0	1.8
		30	22	12	0			6	14	22	30
	-0.8	-0.6	-0.9	-0.1	6.0				-1.5		-0.9
	4.6	4.4	4.7	3.9	3.8				5.3		4.7
	30	27	21	10	0				12		17-30
	-1.8	-1.2	-1.7	-0.9	-0.3	0.0		-0.6	-1.9	-1.2	-1.
	6.0	5.4	5.9	5.1	4.5	4.2		4.8	6.1	5.4	5.
	30	17	16-14	12	7	0		7	13	15	3
	-0.6	-0.4	-0.9	-1.6	-0.7	0.0		-0.3	-1.7	-0.7	+2
	5.5	5.3	5.8	6.5	5.6	4.9		5.2	6.6	5.6	4.
	30	19	15	14-12	9	0		9	12-14	17	3
	-0.1	-0.6	-1.5	-2.1	-0.6	0.0		-0.4	-1.8	-1.1	-0.
	6.0	6.5	7.4	8.0	6.5	5.9		6.3	7.7	7.0	6.
	30	18	16-14	13	8	0		6	13	14	3
1294.5	1295.2	1295.3		1298.2	1298.7		1298.6		1296.0		1296.
6.3	5.5	5.5		2.6	2.1		2.2	4.9		4.1	
30	30	18.0	12.2		0		10.6	FL		30	
		Ditch Bottom									
		0.0	-0.6	0.0				+0.1	+1.0	+2.0	
		3.4	4.0	3.4				3.3	2.4	1.4	
		30	10	0				10	17	30	
	+2.4	+1.9	-1.0	-0.4	0.0			+0.1	-1.1	+2.9	+3.
	4.7	5.2	8.1	7.5	7.1			7.0	8.2	4.2	4.3
	30	18	11	7	0			5	12	24	30
+2.9	+1.5	-0.3	-0.5	-1.1	-0.5	0.0	-0.7	-1.5	-0.7	-0.5	+1.4 +1.
8.1	9.5	11.3	11.5	12.1	11.5	11.0	11.7	12.5	11.7	11.5	9.6
30	18	16	10	9	7	0	12	13	14	17	22 3

	B.S.	H.I.	F.S.	El.
		1300.78		
	3.70	1292.92	11.56	1289.22
154				1287.8
154+56	3' Stone Culvert		Good Condition	1288.0
155				1287.6
156				1289.2
156+59.5	± Road West			1289.4
157	10.41			1289.8
	10.41	1302.70	0.63	1292.29
158				1292.1
159				1295.5
160				1298.6
B.M.			0.78	1301.92

+1.4 -0.7 -1.0 0.0 -0.9 -0.4 0.0 -0.3 -1.1 -0.3 -0.5
3.7 5.8 6.1 5.1 6.0 5.5 5.1 5.4 6.2 5.4 5.6
30 23 15 17 12 10 9 0 11 13 14 30

1284.8

9.7 8.2 8.1 6.2 3.7 5.1 4.9 4.8 3.8 6.4 8.2 6.8
100 30 10.8 9 0 11 13.3 30

-2.0 -1.4 -0.7 -1.0 -0.5 0.0 -0.2 -1.1 -0.4 0.0 +1.2
7.3 6.7 6.0 6.3 5.8 5.3 5.5 6.4 5.7 5.3 4.1
30 22 12 11 10 0 14 15 17 23 30

+1.0 +0.8 0.0 -0.8 -0.2 0.0 -0.7 -1.5 +0.8 +2.3 +2.7
2.7 2.9 3.7 4.5 3.9 3.7 4.4 5.2 2.9 1.4 1.0
30 19 14 12 8 6 13 15 18 23 30

1288.3 1288.7
4.6 4.2 3.5
200 100 0

-0.1 +0.2 -0.3 0.0 -0.2 -1.2 -0.3 +0.5
3.2 2.9 3.4 3.1 3.3 4.3 3.4 3.6
30 12 11 6 11 12 13 30

+1.9 +1.1 -0.2 -0.4 -0.8 -0.5 0.0 -0.4 -1.2 -0.5 -0.3 +2.2 +2.4
8.7 9.5 10.8 11 11.5 11.1 10.6 11 11.8 11.1 10.9 8.4 8.2
30 19 17 12 11 8 0 10 12 13 18 23 30

+1.5 +1.7 +0.8 -1.0 -0.4 0.0 -0.3 -0.8 +1.2 +2.1 +2.6
5.7 5.5 6.4 8.2 7.6 4.2 7.5 8.0 6.0 5.1 4.6
30 15 11 10 7 0 10 12 15 17 30

+1.7 +1.5 -0.6 -0.2 0.0 +0.1 +2.2 +2.7
2.4 2.6 4.7 4.3 4.1 4.0 1.9 1.4
30 15 11 9 0 13 22 30

B.M. Right 160+05 1301.87

	B.S.	H.I.	F.S.	El.
		1302.70		
	3.42	1299.54	6.58	1296.12
161				1295.1
162				1293.3
163				1292.3
164				1290.9
	~~4.60~~	~~1292.24~~	~~11.98~~	~~1287.14~~
165				1289.1
	4.60	1292.24	11.90	1287.64
166				1286.9
167				1282.1
	4.56	1285.75	11.05	1281.19
168				1281.2
				1280.80
168+5	Bes. for Culvert Design Only			

+1.2 +1.1 -0.7 -0.1 0.0 -0.2 -0.6 -0.2 +2.1
3.2 3.3 5.1 4.5 4.4 4.6 5.0 4.6 2.3
30 20 13 8 0 4 6 7 30

-1.1 -0.3 -0.6 -0.2 0.0 00 -0.5 +0.1 -0.4 +0.5
7.3 6.5 6.8 6.4 6.2 6.2 6.7 6.1 6.6 5.7
30 14 13 10 0 5 6 8 15 30

-0.6 -0.1 -0.6 0.0 -0.3 -0.9 +0.2 +1.8
7.8 7.3 7.8 7.2 7.5 8.1 7.0 5.4
30 13 12 0 7 9 10 30

+0.5 +0.4 -0.9 0.0 -0.4 -0.8 +0.1 +1.2 +2.0
8.1 8.2 9.5 8.6 9.0 9.4 8.5 7.4 6.6
30 13 11 0 7 9 11 18 30

+0.5 +0.8 -0.3 0.0 -0.4 -1.2 +0.5 +0.6 +2.2 +2.6
9.9 9.6 10.7 10.4 10.8 11.6 9.9 9.8 8.2 7.8
30 12 10 0 7 11 12 17 21 30

+2.1 +2.3 -0.9 -0.4 0.0 -0.5 -1.5 +3.0 +3.8
3.2 3.0 6.3 5.7 5.3 5.8 6.8 2.3 1.5
30 10 8 5 0 10 12 21 30

+4.5 +2.5 -0.8 -0.3 0.0 +0.2 -0.1 -0.8 -0.1 +0.3 +3.8 +5.8
5.6 7.4 10.9 10.4 10.1 9.9 10.3 10.9 10.2 9.8 6.3 4.3
30 9 5 3 0 6 13 14 15 18 23 30

-4.1 -1.9 -0.4 0.0 -0.1 -3.5 -1.5 -1.7
8.7 6.5 5.0 4.6 4.7 8.1 6.1 6.3
30 11 6 0 9 16 18 30

1271.3 1273.7 1277.9 1280.7 1280.8 1280.6 1278.2 1274.2 1276.1
14.5 12.1 7.9 5.1 5.0 5.2 7.6 11.6 9.7
100 8.8 0 12.7 60

		1285.75		
169				1282.1
	9.60	1295.27	0.08	1285.67
			9.10	1286.17
170				1285.8
171				1286.8
172				1288.4
173				1290.3
173+40				1291.3
174				1289.8
175				1284.0
	0.37	1282.95	12.69	1282.58
			1.75	1281.20

+3.0 +3.0 -0.5 -0.2 0.0 -0.3 -1.1 +2.7 +3.1
0.7 0.7 4.2 3.9 3.7 4.0 4.8 1.0 0.6
30 15 13 6 0 7 8 25 30

B.M. Left, 169+50 (1286.14)

-1.3 -0.2 -0.8 -0.3 0.0 -0.2 -1.3 -0.6 -0.3 +1.3 +1.5
10.8 9.7 10.3 9.8 9.5 9.7 10.8 10.1 9.8 8.2 8.0
30 13 12 10 0 7 8 9 16 21 30

+0.2 -0.5 -0.4 -0.9 -0.2 0.0 -0.2 -0.8 +0.6 +1.4
8.3 9.0 8.9 9.4 8.7 8.5 7.7 9.3 7.9 7.1
30 22 13 12 6 0 5 9 12 30

+0.3 +0.3 -1.0 -0.4 0.0 -0.8 +1.2 +2.4
6.6 6.6 7.9 7.3 6.9 7.9 5.7 4.5
30 13 12 5 0 8 11 30

+0.5 +0.3 -0.8 -0.2 0.0 -0.2 -0.6 +1.1 +2.7
4.5 4.7 5.8 5.2 5.0 5.2 5.6 3.9 2.3
30 11 10 7 0 8 9 12 30

+0.1 -0.3 -1.1 -0.3 0.0 -0.5 -0.9 +0.9 +1.7
3.9 4.3 5.1 4.3 4.0 4.5 4.9 3.1 2.3
30 11 10 5 0 9 10 12 30

+1.5 +1.1 -1.5 -0.2 0.0 -0.5 -1.4 +2.0 +3.1
4.0 4.4 7.0 5.7 5.5 6.0 6.9 3.5 2.4
30 14 11 5 0 8 10 15 30

+3.3 +3.3 -1.4 -0.5 0.0 -0.4 -1.1 -0.1 +5.2 +6.1
8.0 8.0 12.7 11.8 11.3 11.7 12.4 11.4 6.1 5.2
30 17 9 7 0 9 10 13 20 30

B.M. Left 176+50 (1281.13)

1282.95

175+65			3.7	1279.3
176				1278.1
				1277.1
176+80	Section for Culvert Design Only			
177				1276.7
178				1278.3
	11.98	1294.06	0.87	1282.08
179				1282.1
180				1287.2
	6.53	1300.28	0.31	1293.75
181				1292.6
182				1296.3
183				1294.6
183+35	Section for Culvert Design only			1294.6

+4.5 +3.2 +3.6 -0.3 -1.0 -0.5 0.0
0.4 1.7 1.3 5.1 5.9 5.4 4.9
30 24 18 11-8 7 4 0

1270.6 1271.1 1272.1 1274.1 1276.3 1277.1
12.4 11.9 10.9-8.9-6.7 5.9
100 30 8.9 6-0-9

-4.0 -2.6 -1.0 -1.2 -0.4 0.0
10.3 8.9 7.3 7.5 6.7 6.3
30 17 11 10-8 6 0

+3.6 -0.1 -0.2 -1.1 -0.4 0.0
1.1 4.8 4.9 5.8 5.1 4.7
30 22 14 12 9 0

+3.8 +3.6 +2.9 +0.7 -0.8 -0.3 +0.1 0.0
8.4 9.1 11.3 12.8 12.3 11.9 12.0
28 20 14 12 9 5 0

+3.6 +2.8 +1.2 -1.0 -0.2 0.0
3.3 4.1 5.7 7.9 7.1 6.9
30 20 18-15 12 9 0

+1.1 +1.0 +0.2 -1.2 -0.3 0.0
6.6 6.7 7.5 8.9 8.0 7.7
30 16 13 12 9 0

+1.3 +1.9 -0.6 -0.3 0.0
2.7 2.1 4.6 4.3 4.0
30 15 10 8 0

-0.7 -1.2 -0.3 -0.7 -0.3 0.0
6.4 6.9 6.0 6.4 6.0 5.7
30-25 18 11 9 6 0

1292.9
10.4 7.8 7.4 6.1 5.7
100 30 8 0

-0.3 -0.6 -0.3 +0.8 +0.9 +1.2
5.2 5.5 5.2 4.1 4.0 0.7
11 12 13 17 24 30

1276.3 1274.0 1271.8 1272.8
6.7-9.0-11.2 10.2
14.2 50

-0.2 -1.1 -1.7 -1.7 -2.8
6.5 7.4 8.2 8.0 9.1
9 17 20 22 30

-0.6 -1.1 -0.4 0.0 +3.9
5.3 5.8 5.1 4.7 0.8
6 9 10 20 30

-2.3 -1.1 +2.6 +2.4
12.3 13.1 9.4 9.6
5 7 15 30

-0.3 -0.9 +3.7 +4.0 +3.2
7.2 7.8 3.2 2.9 3.7
4 5 12 20 30

-0.4 -0.9 +2.3 +3.1
8.1 8.6 5.4 4.6
4 6 11 30

-0.2 -0.7 +3.0 +3.3 +3.0
4.2 4.7 1.0 0.7 1.0
7 9 13 26 30

-0.5 -1.1 -0.5 +1.2 +1.1
6.2 6.8 6.2 4.5 4.6
12 14 15 26 30

6.0-7.8
11

5.7
30

		1300.28		
184				1293.7
184+75				1294.4
185			6.7	1293.6
	5.23	1292.76	12.75	1287.53
186				1287.6
187				1281.9
	1.80	1281.69	12.87	1279.89
188				1276.9
188+50			7.6	1274.1
189				1270.0
189+40			15.8	1265.9
	0.79	1269.53	12.95	1268.74
190				1263.7
191				1260.9
192				1258.7

-1.2 -0.2 -0.6 0.0 | -0.2 -0.8 0.0 +2.4 +3.1
7.8 6.8 7.2 6.6 | 6.8 7.4 6.6 4.2 3.5
26 14 10 0 | 11 13 14 24 30

-1.1 -0.8 -0.4 +0.4 -1.0 -0.4 0.0 | -0.3 -0.9 +1.2 +2.1 +3.5 +3.7
7.0 6.7 6.3 5.5 6.9 6.3 5.9 | 6.2 6.8 4.7 3.8 2.9 2.2
30 26 18 10 9 7 0 | 10 12 14 18 24 35

-0.2 +0.8 +1.0 +0.4 -1.2 -0.6 0.0 | -0.5 -1.2 +2.4 +3.7
6.9 5.9 5.7 6.3 7.9 7.3 6.7 | 7.2 7.9 4.3 3.0
30 25 19 10 8 5 0 | 9 11 16 30-35

+2.4 +1.2 -1.8 -0.8 0.0 | -0.7 -1.2 +4.2 +5.2
2.8 4.0 7.0 4.0 5.2 | 5.9 6.4 1.0 0.0
30-25 12 9 7 0 | 8 10 20 30

+2.7 +3.2 +2.4 -1.2 -0.4 0.0 | -0.5 -1.3 +2.9 +4.7
8.2 7.7 8.5 12.1 11.3 10.9 | 11.4 12.2 8.0 6.2
30 28 14 8 5 0 | 9 11 18 30

+1.5 +2.2 -1.3 -0.7 0.0 | -0.1 -0.6 +2.5 +3.3 +4.0
3.3 2.6 6.1 5.5 4.8 | 4.9 5.4 2.3 1.5 0.8
30 14 8 5 0 | 9 12 18 25-30

+4.7 +5.6 -1.0 -0.2 0.0 | 0.0 -1.3 +6.5 +7.0 +7.7
7.0 6.1 12.7 11.9 11.7 | 11.7 13.0 5.2 4.7 4.0
30 28-15 7 5 0 | 7 10 22 25 30

+6.4 +5.9 +5.0 +2.7 -0.1 -1.1 -0.4 0.0 | -0.5 -1.0 +2.1 +2.3 +3.6
0.2 1.2 1.9 8.1 5.9 6.9 6.2 5.8 | 6.3 6.8 3.7 3.5 3.2
30 26 20 16 11-9 8 6 0 | 9 11 18 22 30

+3.1 +1.6 -0.6 -0.2 -0.4 0.0 | -0.2 -0.9 0.0 -1.4
5.5 7.0 9.2 8.5 9.0 8.6 | 8.8 7.5 8.6 10.0
30 26 15 9 8 0 | 9 12 13 20-25

-0.5 0.0 | 0.0 -0.7 -0.1 -1.1 -1.0
11.3 10.8 | 10.8 11.5 10.9 11.9 11.8
26 0 | 11 13 14 20 25

		1269.53		
	4.38	1261.13	12.78	1256.75
193				1257.5
193+50				1252.7
194				1248.6
	2.30	1250.81	12.62	1248.51
195				1245.1
195+66				1245.3
196				1244.1
			1.69	1249.12
197				1244.1
198				1244.3
199				1241.4

+5.6 +3.6 +1.7 +0.1 0.0

+2.0 0.0 1.9 3.5 3.6

30 20 9 6 0

−0.7 −2.2 −1.0 −1.7

4.3 5.8 4.6 5.3

13 16 19 25

+8.4 +7.4 −0.2 0.0

0.0 1.0 8.6 8.4

30 16 7 0

−0.1 −2.4 +2.7

8.5 10.8 5.7

13 15 22-25

+9.5 +9.0 +3.9 −0.7 −0.2 0.0

3.0 3.5 8.6 13.2 12.7 12.5

30 25 13 9 6 0

−0.2 −1.6 +1.2 +4.4

12.7 14.1 11.3 11.1

13 15 20 25

−0.4 −1.2 −0.3 −1.2 −0.5 0.0

6.1 6.9 6.0 6.9 6.2 5.7

30 19 14 13 11 0

−0.4 −1.6 −0.8 −0.5

6.1 7.3 6.3 6.2

10 12 13 25

12.92.5

10.0 8.1 8.0 7.2 4.8 5.9 5.5 5.5 4.2 6.6-8.7 1.5

100 30 14 12.5 0 13.3 15 30

−1.5 −0.6 −1.1 0.0

8.2 7.3 7.8 6.7

30 19 16 0

7.7

−0.3 −0.8 −0.4

7.0 7.5 7.1

23 24 25

B.M. Right 196 + 45

1248.96

−0.6 −0.4 −1.4 −0.7 0.0 0.0

7.3 7.7 8.1 7.4 6.7 6.7

30 19 18 16 7 0

0.0 6.7 5

−0.6 +1.1 +2.2

7.3 5.6 4.5

10 12 25

+0.7 +0.2 −1.8 −0.5 +0.1 0.0

5.8 6.3 8.3 7.0 6.4 6.5

30 20 18 14 5 0

−0.7 −2.3 +1.2 +2.0

7.2 8.8 5.3 4.5

4 8 13 25-30

+1.5 +1.2 −0.9 −0.4 +0.2 0.0

7.9 8.1 10.3 9.8 9.2 9.4

30 14 18 15 5 0

−0.8 +2.4 +3.0

10.2 7.0 6.4

9 14 25-30

		1250.81		
200				1240.5
	6.87	1246.77	10.91	1239.90
			12" or 15" Pipe Required.	
200+18	Section for Culvert Design only			1240.85
201				1241.3
201+15			5.2	1241.6
202				1241.4
203				1241.2
			3.05	1243.72
	0.18	1243.69		1243.51
203+75			2.1	1241.6
204				1241.2
205				1237.2
206				1233.7
	3.00	1234.44	12.25	1231.44

-1.7	-1.4	-0.6	-1.6	-0.5	0.0	-0.1	-0.5	-1.4	-0.7	-1.5
12.0	11.7	10.9	11.9	10.8	10.3	10.4	10.8	11.7	11.0	11.8
30	24	19	18	15	0	5	9	10	11	25
1234.11	1237.2	1237.2	1240.2	1240.5		1240.2	1237.5	1237.1	1238.9	1238.8
12.7	9.6	9.6	6.6	6.3		6.6	9.3	9.7	7.9	8.0
100	30		16	0		5.5		11.7	14	30
								11.7		
+1.4	+1.8	-1.3	-0.7	+0.1	00	-0.5	-1.9	+1.7	+2.2	
3.9	3.7	6.8	6.2	5.4	5.5	6.0	7.4	3.8	3.3	
30	18	15	13	4	0	7	11	16	25-30	
-1.2	-0.7	-1.4	-0.6	00		-0.8	-1.5	-0.6	+0.5	
6.6	6.1	6.8	6.0	5.4		6.2	6.9	6.0	4.9	
30	17	15	13	0		11	12	14	25-30	
-0.3	-0.1	-.1	-0.3	00		-0.4	-0.9	-0.2	+0.5	
5.9	5.7	6.7	5.9	5.6		6.0	6.5	5.8	5.1	
30	18	16	14	0		10	12	13	25-30	

B.M. Rt. Sta. 204+75 1243.51

Mar. 26, 1925 Fair. Marks, Grau, Sprague

+1.8	+1.2	-1.0	-0.3	00		-0.4	+1.0	+2.0	+1.5	
0.7	1.3	3.5	2.8	2.5		2.9	1.5	0.5	+1.0	
30	18	14	11	0		8	9	18	30	
+2.5	+1.6	-.1	-0.1	00		-0.3	-1.8	+0.6	+3.1	+2.9
4.0	4.9	7.6	6.6	6.5		6.8	7.3	5.9	3.4	3.6
30	16	11	5	0		7	9	11	25	30
+1.5	+1.9	-1.0		00		-0.7	-1.6	+2.5	+2.8	+4.0 +4.3
8.5	8.1	11.0		10.0		10.7	11.6	7.5	7.2	6.0 5.5
30	15	11		0		6	8	14	21	25 30

	1234.44			
207				1229.2
208				1224.1
209				1221.4
	0.80	1223.74	11.50	1222.94
210				1220.1
210+14.3	Section for Culvert Design Only Condition Fair, Outlet Required			1219.7
211				1218.6
212				1218.9
213				1219.8
213+75				1221.5
214				1220.1
214+50			5.7	1218.0

+3.1 +2.6 -0.7 -0.2 +0.1 00
2.1 2.6 5.9 5.3 5.1 5.2
30 18 14 10 7 0

-0.1 -0.9 +4.0 +5.0 +5.1
5.3 6.1 1.2 0.2 0.1
4 6 12-21 25 30

+3.3 +2.3 +0.3 -0.6 +0.2 00
7.0 8.0 10.2 10.9 10.1 10.3
30 20 18-17 16 8 0

-0.2 -0.9 +3.6 +3.8 +4.7
10.5 11.2 6.7 6.5 5.6
2 4 12 20 25-30

+0.6 -0.1 -1.0 -0.3 0.0 00
12.4 13.1 14.0 13.3 13.0 13.0
30 16 15 13 10 0

-0.5 0.0 +0.7 +0.7
13.5 13.0 12.3 12.3
4 5 13 30

-1.8 -0.9 -1.8 -0.2 00
5.5 4.6 5.5 3.9 3.7
30-28 17 15 11 0

0.0 -2.9 -1.2 -1.9 -1.5
3.7 6.6 4.9 5.6 5.2
4 9 11 22 30

1214.8 1216.3 1217.1 1218.1 1220.3 1219.6 1219.6 1219.6 1220.3 1218.1 1216.9 1217.4
8.9 7.4 6.6 5.6-3.4 4.1 4.1 4.1 3.4 5.6- 6.8 6.3
100 30 13.1 11.5 0 6 7.5 30

+0.3 -0.1 -0.9 -0.4 -0.1 00
4.9 5.3 6.1 5.6 5.1 5.2
30 18 17 15 6 0

-0.3 -1.0 +0.1 +1.5
5.5 6.2 5.1 3.7
5 6 7 30

+0.1 -0.2 -1.0 -0.4 +0.2 00
4.8 5.1 5.9 5.3 4.7 4.9
30 18 17 16 7 0

-0.2 -0.8 +0.8 +0.9 +1.9
5.1 5.7 4.1 4.0 3.0
2 4 6 19 30

+0.5 -0.2 -0.9 -0.4 +0.2 00
3.5 4.2 4.9 4.4 3.8 4.0
30 18 17 15 7 0

-0.1 -0.7 +1.3 +2.5
4.1 4.7 2.7 1.5
3 4 7 30

+1.5 +0.5 -0.8 -0.3 +0.3 00
0.8 1.8 3.1 2.6 2.0 2.3
30 17 16 15 7 0

-0.3 -0.8 +0.8 +1.5 +1.3
2.6 3.1 1.5 0.8 1.0
4 5 8 17 30

+1.8 +0.6 -0.9 -0.3 +0.1 00
1.9 3.1 4.6 4.0 3.6 3.7
30 17 16 14 7 0

-0.3 -0.7 +1.9 +2.5 +2.1
4.0 4.4 1.8 1.2 1.6
3 5 8 2.0 30

		1223.7+		
215				1216.9
	2.23	1218.31	7.66	1216.08
216				1215.7
217				1213.9
218				1211.8
219				1210.5
220				1209.6
221				1209.2
	3.95	1212.74	9.32	1208.99
			2.07	1210.87
222				1208.9
223				1208.4

+1.3 +0.2 -0.8 0.0 00

5.6/30 6.7/16 7.7/15 6.9/13 6.9/0

-0.2 -1.0 +0.9 +0.5 +0.8

7.1/4 7.9/5 6.0/9 6.4/23 6.1/30

-0.1 -0.4 -1.1 -0.1 00

2.7/28 3.0/16 3.7/15 2.7/14 2.6/0

0.0 -1.1 -0.2 -0.8 -0.4

~~2.8~~/0 2.6/3 3.7/5 2.8/7 3.4/23 3.0/30

+2.9 +1.0 -0.3 +0.2 00

1.5/30 3.4/16 4.7/13 4.2/12 4.4/0

-0.1 -0.9 +0.8 -1.4 -1.6

4.5/5 5.3/7 3.6/9 3.0/19 2.8/30

+2.3 +0.8 -0.7 0.0 0.0

4.2/30 5.7/17 7.2/14 6.5/13 6.5/0

-0.3 -1.0 +0.9 +1.9

6.8/6 7.5/7 5.6/9 4.6/30

+0.6 -0.3 -0.2 -0.7 0.0 00

7.2/29 8.1/23 8.0/15 8.5/14 7.8/12 7.8/0

-0.2 +0.8 -0.2 +0.1

8.0/5 8.6/6 8.0/8 7.7/23 Fence

Hedge

-0.2 -0.3 -0.8 00 · 00

8.9/28 9.0/13 9.5/12 8.7/10 8.7/0

-0.2 -0.9 +0.1 -0.7

8.9/7 9.6/8 8.6/9 9.4/25 fence

Hedge

-0.3 -0.2 -1.0 -0.2 00

9.4/30 9.3/12 10.1/11 9.3/10 9.1/0

-0.1 -1.0 -0.7

9.2/7 10.1/8 9.8/26 Fence

B.M. Left, 222+90 (1210.83)

-0.5 -0.6 -1.2 -0.5 00

4.5/30 4.6/12 5.2/11 4.5/9 4.0/0

-0.3 -1.2 -0.3 -0.7

4.3/8 5.2/10 4.3/4 4.7/28 Fence

+0.6 -0.4 -1.6 -0.6 00

3.6/30 4.6/14 5.8/13 4.8/11 4.2/0

-0.6 -1.6 -0.6 +0.7 +1.6

4.8/8 5.8/10 4.8/11 3.5/20 2.6/29

1212.94

224 — 1207.5

225 — 1206.0

226 — 1205.4

227 — 1204.8

3.84 — 1204.88 — 11.90 — 1201.04

228 — 1201.6

229 — 1200.3

Section for Culvert Design Only

29+55 — 1200.3

230 — 1200.0

231 — 1201.0

232 — 1199.6

+0.8 −0.4 −1.3 −0.6 00

4.6 | 5.8 | 6.7 | 6.0 | 5.4

30 – 26 | 19 – 12 | 10 | 8 | 0

−0.8 −1.6 −0.6 +1.2 +1.6

6.2 | 7.0 | 6.0 | 4.1 | 3.8

8 | 10 | 11 | 22 | 18.5 fence

+0.1 −0.4 −1.1 −0.3 00

6.8 | 7.3 | 8.0 | 7.2 | 6.9

30 – 27 | 9 | 8 | 6 | 0

−0.3 −1.1 −0.4 −0.4 +1.1

7.2 | 8.0 | 7.3 | 7.3 | 5.8

10 | 11 | 12 | 20 | 29

−0.7 −0.3 −1.2 +0.2 0.0

8.2 | 7.8 | 8.7 | 7.7 | 7.5

30 | 8 | 7 | 5 | 0

0.0 −0.9 −0.2 −0.4

7.5 | 8.4 | 7.7 | 7.7

11 | 13 | 14 | 29 fence

+1.1 0.0 −1.2 0.0 00

7.0 | 8.1 | 9.3 | 8.1 | 8.1

30 – 25 | 7 | 6 | 4 | 6

−0.5 −1.5 +0.4 +1.3

8.6 | 9.6 | 7.7 | 6.8

7 | 13 | 16 | 38

+2.8 +0.7 −0.5 −0.1 00

0.5 | 2.6 | 3.8 | 3.4 | 3.3

30 | 6 | 4 | 2 | 0

−0.3 −1.0 +0.8 +1.9 +2.1

3.6 | 4.7 | 2.5 | 1.4

13 | 15 | 17 | 21

−0.6 −0.7 −0.1 −0.8 −0.1 00

5.0 | 5.3 | 4.7 | 5.4 | 4.7 | 4.6

30 | 16 | 6 | 4 | 3 | 0

+0.2 −0.1 −0.9 −0.2

4.4 | 4.7 | 5.5 | 4.8 | 4.8

4 | 12 | 14 | 15 | 30

1196.4 — 1197.4 — 1198.3 — 1197.2 — 1198.5 — 1199.7 — 1199.9 — 1200.3

8.5 | 7.5 | 6.6 | 7.7 | 6.4 | 5.2 | 5.0 | 4.6

100 | 30 | 10 | 8 | 6 | 0

1200.3 — 1199.9 — 1198.7 — 1198.0 — 1198.3

4.6 | 5.0 – 6.2 – 6.9 | 6.5

9 | 11.5 | 30

−0.5 −0.8 −0.8 −0.4 00

5.4 | 5.7 | 5.7 | 5.3 | 4.9

30 | 11 | 9 | 7 | 0

−0.2 −1.0 +0.6 +1.4

5.1 | 5.9 | 4.3 | 3.5

8 | 12 | 16 | 25-30

+0.7 +0.1 −0.9 −0.4 00

3.2 | 3.8 | 4.8 | 4.3 | 3.9

30 | 8 | 7 | 5 | 0

+0.2 −0.1 −0.6 +0.7 +1.4

3.7 | 4.0 | 4.5 | 3.2 | 2.5

3 | 10 | 11 | 12 | 30

+1.1 +0.4 −1.0 −0.5 00

4.2 | 4.9 | 6.3 | 5.8 | 5.3

30 | 8 | 6 | 5 | 0

−0.2 −0.7 +0.7 +1.6

5.5 | 6.0 | 4.6 | 3.7

11 | 12 | 14-19 | 30

		1204.88		
233				1197.5
234				1195.3
235				1193.0
	1.93	1195.21	12.60	1192.28
235+44				
236				1190.2
236+90				
237				1188.0
			1.08	1194.13
	1.08	1195.14		1194.06
	5.43	1190.01	10.56	1184.58
238				1184.9
239+80	Set for Earthwork			1184.1

+1.2 +1.4 +0.2 -1.0 -0.4 00 +0.3 -0.2 -0.7 +0.7 +1.9

6.2 / 30 | 6.0 / 12 | 7.2 / 6 | 8.4 / 5 | 7.8 / 4 | 7.4 / 0 | 7.1 / 4 | 7.6 / 12 | 8.1 / 14 | 6.7 / 16 | 5.5 / 30

+1.1 +0.4 -1.0 -0.5 00 +0.1 -0.2 -0.9 +0.8 +1.7 +1.9

8.5 / 30−12 | 9.2 / 8 | 10.6 / 7 | 10.1 / 5 | 9.6 / 0 | 9.5 / 4 | 9.8 / 7 | 10.5 / 13 | 8.8 / 15 | 7.9 / 20 | 7.7 / 30

+2.2 +1.7 -0.3 -1.5 -0.7 00 -0.5 -1.4 +0.1 +1.6 +2.6

9.7 / 30 | 10.2 / 16 | 12.2 / 12-9 | 13.4 / 8 | 12.6 / 6 | 11.9 / 0 | 12.4 / 10 | 13.3 / 12 | 11.8 / 14 | 10.3 / 18 | 9.3 / 30

1190.6
4.6
11

+2.8 +0.4 -0.8 -0.2 00 -0.1 +0.3 +1.5

3.0 / 30 | 4.6 / 11 | 5.8 / 9 | 5.2 / 8 | 5.0 / 0 | 5.1 / 9 | 4.2 / 10 | 3.5 / 30

1186.9
8.3
9.5

+3.1 +2.8 +1.0 +0.2 -1.1 -0.4 00 -0.4 -1.1 0.0 +2.4

4.1 / 30 | 4.4 / 19 | 6.2 / 15 | 7.0 / 11 | 8.3 / 9 | 7.6 / 8 | 7.2 / 0 | 7.6 / 8 | 8.3 / 9 | 7.2 / 11 | 9.8 / 30

B.M. Right 236+50 (1194.06)

+2.9 -0.4 -0.2 -0.7 -0.4 00 -0.1 -0.3 0.0 0.5

2.2 / 29 fence | 5.5 / 14 | 5.3 / 9 | 5.8 / 8 | 5.5 / 6 | 5.1 / 0 | 5.2 / 8 | 5.4 / 10 | 5.1 / 12 | 5.1 / 30

-2.2 -1.6 -2.6 -1.4 -0.2 00 00 -2.6 -1.6 -2.6

8.1 / 30 | 7.5 / 13 | 8.5 / 11 | 7.3 / 9 | 6.1 / 6 | 5.9 | 5.9 / 9 | 8.5 / 16 | 7.5 / 17 | 8.5 / 27 fence

				1190.01
				Sidewalls caved
239				Section for Culvert Design
				Culvert in fair condition, can be extended
				but it is advisable to build new culvert.
239+75				1184.6
240			4.8	1185.2
240+25				1185.8
	11.63	1200.18	1.46	1188.55
241				1189.2
242				1193.2
243				1196.6
243+65				1198.8
244				1197.8
	1.29	1196.41	5.06	1195.12
245				1194.8
246				1191.6

1179.1 1179.8 1179.1 1183.0 1184.4 1184.1 1184.2 1182.0 1178.3 1179.9

10.9 10.2 10.9 8.0 5.6 5.9 5.8 8.0 11.7 10.1

100 30 8.9 0 12 30

-0.6 -1.3 -0.3 -0.7 00 00 -0.1 -0.8 -0.4 -1.2 -1.4

6.0 5.7 5.7 6.1 5.4 5.4 5.5 6.2 5.8 6.6 6.8

30 26 6 5 2 0 12 14 15 28 30

+1.2 +1.2 -0.5 00 +0.1 -0.2 -0.9 +3.0 +3.7

0.0 0.0 4.7 4.2 4.1 4.9 5.1 1.2 +0.5

28 11 4 0 6 11 15 23 30

+3.0 +3.3 +2.8 -0.8 -0.4 00 +0.1 -0.4 -1.0 +2.7 +3.5

8.0 7.7 8.2 11.8 11.4 11.0 10.9 11.4 12.0 8.3 7.5

30 14 9 4 3 0 7 13 14 20 30

+4.1 +3.2 -0.6 -0.4 00 +0.1 -0.4 -1.0 +2.8 +3.7

2.9 3.8 7.6 7.4 7.0 6.9 7.4 8.0 4.2 3.3

30 12 6 5 0 4 10 12 19 30

+2.5 +1.1 -0.2 00 +0.2 -0.3 -0.9 +1.8 +2.5 +2.2

1.1 2.5 3.8 3.6 3.4 3.9 4.5 1.8 1.1 1.4

30-25 11 8 0 3 10 11 17 23 30

+1.3 +1.0 -0.4 00 -0.4 -0.9 +0.8 +1.4

0.1 0.4 1.8 1.4 1.8 2.3 0.6 0.0

30 11 8 0 8 10 12 30

+1.8 +1.5 -0.7 -0.3 00 -0.4 -1.0 +1.3 +2.2

0.6 0.9 3.1 2.7 2.4 2.8 3.4 1.1 0.2

27 12 10 9 0 7 8 13 30

+1.7 +0.8 -0.8 -0.2 00 -0.2 -0.8 +0.7 +1.6

0.4 0.8 2.4 1.8 1.6 1.8 2.4 0.9 0.0

30 14 12 11 0 6 7 10 30

+2.4 +1.9 -0.4 00 -0.1 -0.6 +1.8 +2.1 +2.0

2.4 2.9 5.2 4.8 4.9 5.4 3.0 2.7 2.8

30 16 12 0 7 8 13 24 30

		1196.41		
247				1186.6
248				1182.7
			9.69	1186.72
	0.19	1184.81	11.79	1184.62
249				1179.3
250				1177.2
251				1175.4
252				1173.8
	2.62	1176.40	11.03	1173.78
253				1172.1
254				1169.6
255				1166.9

+2.6 +2.0 −0.6 00 | −0.2 −0.7 +3.8 +4.3
7.2 7.8 10.4 9.8 | 10.0 10.5 6.0 5.5
30 17 13 0 | 5 7 16 30

+3.0 +1.2 −0.8 −0.4 +0.1 00 | −0.4 −0.8 +0.2 +3.0
10.7 12.5 14.5 14.1 13.6 13.7 | 14.1 14.5 13.5 10.7
30 17 14 13 5 | 3 5 8 30

B.M. Right 247+90 (1186.69)

+2.1 +1.9 −0.6 −0.2 00 | 00 −0.3 +0.5 +2.4
3.4 3.6 6.1 5.7 5.5 | 5.5 5.8 5.0 3.1
30 19 15 13 0 | 3 4 7 30

+0.5 −0.1 −0.7 +0.1 00 | +0.1 −0.5 +0.1 +0.6
7.1 7.7 8.3 7.5 7.6 | 7.5 8.1 7.5 7.0
30 14 13 11 0 | 4 6 9 30

−0.3 −0.2 −1.0 00 00 | 00 −0.7 −0.2 −0.8
9.7 9.6 10.4 9.4 9.4 | 9.4 10.1 9.6 10.2
30 15 14 12 0 | 4 5 7 30

00 00 −1.1 00 00 | 00 −0.7 −0.1 −1.1
11.0 11.0 12.1 11.0 11.0 | 11.0 11.7 11.1 12.1
30 14 13 12 0 | 4 5 7 30

+1.3 +1.0 −0.9 00 +0.2 00 | 00 −0.6 +0.3 +0.1
3.0 3.3 5.2 4.3 4.1 4.3 | 4.3 4.9 4.0 4.2
30 16 14 12 5 0 | 4 5 7 30

+3.0 +2.8 0.8 −0.3 00 | −0.1 −0.4 +1.2 +2.3 +2.7
3.8 4.0 7.6 7.1 6.8 | 6.9 7.2 5.6 4.5 4.1
30 15 11 10 0 | 5 6 11 19 30

+1.8 +1.7 −0.9 −0.3 00 | −0.1 −0.4 +0.8 +2.6 +3.1
7.7 7.8 10.4 9.8 9.5 | 9.6 9.9 8.7 6.9 6.4
30 15 12 10 0 | 5 6 8 21 30

		1176.40		
256				1164.7
			8.51	1167.89
	0.26	1164.77	11.89	1164.51
257				1162.2
258				1157.7
259				1154.8
260				1153.2
	5.40	1159.37	10.80	1153.97
260+63				1153.0
261				1152.2
262				1152.7
263				1154.8

1148.2
11.4
200

1161.1 1163.4

−1.3 +0.2 00 00 −0.7 +0.4 +0.4 +1.9 +2.6

15.3 13.0 11.5 11.7 11.7 12.4 11.3 11.3 9.8 9.1

100 30 11 0 6 8 9 15 19 27

B.M. Left 255 + 85 (1167.82)

+2.6 +2.0 −0.6 −0.1 00 00 −0.3 −0.8 +0.5 +2.1 +2.4

0.0 0.6 3.2 2.7 2.6 2.6 2.9 3.4 2.1 0.5 0.2

27 14 11 10 5 0 6 8 9 15 30

+3.5 +3.1 −0.6 −0.1 00 00 −0.8 +3.1 +4.1

3.6 4.0 7.7 7.2 7.1 7.1 7.9 4.0 3.0

27 18 11 10 0 5 6 19 30

+0.8 +0.3 −0.3 −0.9 −0.1 00 −0.2 −0.6 +0.9 +1.7

9.9 9.7 10.3 10.9 10.1 10.0 10.2 10.6 9.1 8.3

26 17 14 13 11 0 7 9 14 30

+0.3 −0.5 −1.2 −0.1 00 +0.1 −0.4 +1.1

11.3 12.1 12.8 11.7 11.6 11.5 12.0 10.5

27 13 12 11 0 8 9 30

1149.8 1150.8 1150.6 1152.0 1153.9 1153.0 1153.0 1153.0 1154.0 1151.9 1150.2 1151.4

9.6 8.6 8.8 7.4 5.5 10.7 H.W. 6.4 6.4 6.4 8.5 5.4 7.5 9.2 10. H.W. 8.0

100 30 9 0 8.5 30

−1.4 00 −0.3 −1.2 −1.2

8.6 7.2 7.5 8.4 8.4

27 0 10 11 30

+1.8 +0.9 −0.3 00 00 −0.7 +0.7 +1.7

4.9 5.8 7.0 6.7 6.7 7.4 6.0 5.0

29 13 11 0 12 14 16 25-30

+1.2 +0.5 −0.9 −0.2 00 −0.4 −1.0 +0.6

3.4 4.1 5.5 4.8 4.6 5.0 5.6 4.0

29 11 9 8 0 13 14 22-30

		1159.37		
	5.02	1161.32	3.07	1156.30
264				1156.0
265				1156.9
266				1156.9
267			~~4.71~~	1156.0
T.P.			4.71	1156.61
	2.12	1158.73		1156.61
268				1155.8
269				1155.0
270				1153.2
271				1151.6
272				1150.9
	3.95	1155.07	7.61	1151.12

+0.7 +0.2 -1.2 -0.3 00 — -0.4 -1.1 0.0 +1.3

4.6/25 5.1/11 6.5/10 5.6/8 5.3/0 — 5.7/13 6.4/14 5.3/15-18 4.0/25-20

00 -0.2 -1.0 -0.3 00 — -0.4 -1.1 -0.3 +0.1 +0.8

4.4/25 4.6/11 5.4/10 4.7/8 4.4/0 — 4.8/12 5.5/14 4.7/15 4.3/22 3.6/25

+0.3 -0.3 -1.0 -0.3 00 — -0.4 -1.1 -0.4 -0.1 +0.4

4.1/25 4.7/11 5.4/10 4.7/9 4.4/0 — 4.8/12 5.5/13 4.8/14 4.5/22 4.0/25

+0.8 +0.4 -0.4 -1.1 -0.4 00 — -0.3 -1.0 -0.5 -0.1 +0.5

4.5/25 4.7/15 5.7/10 6.4/9 5.7/8 5.3/0 — 5.6/12 6.3/13 5.8/14 5.4/22 4.8/25

Hub, 25' Right of ℄, Sta 267+00

Mar. 28, 1925, Fair. Windy, Marks, Graw, Sprague

-0.3 +0.1 -0.5 -1.3 -0.5 0.0 — -0.2 -1.0 -0.4 -0.4 +0.1

3.2/25 2.8/18 3.4/10 4.2/9 3.4/7 2.9/0 — 3.1/13 3.9/14 3.3/16 3.3/22 2.8/25

+1.3 +0.7 -0.9 -0.3 0.0 — -0.2 -0.8 +0.1 +0.6 +1.2

2.4/25 3.0/11 4.6/8 4.0/6 3.7/0 — 3.9/13 4.5/14 3.6/15 3.1/23 2.5/25

+1.0 +1.0 -0.9 -0.2 0.0 — 0.0 -0.4 +0.3 +1.1

4.5/25 4.5/10 6.4/7 5.7/5 5.5/0 — 5.5/13 5.9/15 5.2/16-22 4.4/25

+1.8 +0.9 +0.6 -0.7 -0.2 0.0 — +0.1 -0.6 +0.3 +1.

5.3/25 6.2/10 6.5/9 7.8/7 7.3/5 7.1/0 — 7.0/13 7.7/15 6.8/16 5./25

+0.6 -0.4 -1.1 -0.3 0.0 — -0.2 -1.0 -0.5 -0.6 0.0

7.2/25 8.2/9 8.9/8 8.1/7 7.8/0 — 8.0/12 8.8/14 8.3/15 8.4/23 7.8/25

		1155.07		
273				1150.8
273+22				1151.1
274				1150.9
			1.19	1153.88
275				1151.2
276				1149.4
277				1147.1
278				1145.3
	2.20	1148.56	8.71	1146.36
279				1144.3
279+80				1143.7

-0.1 -1.2 -0.7 -1.4 -0.2 0.0
4.4 5.5 5.0 5.7 4.5 4.3
25 20 10 9 7 0

1146.4 1148.2 1149.5 1151.2 1151.1
8.7 6.7 5.6 5.0 3.7 4.0
200 100 30 10 6.5 0

-0.4 -0.7 -1.4 -0.4 0.0
4.6 4.9 5.6 4.6 4.2
25 14 13 11 0

B.M., Right 274+15 (1153.88)

0.0 +0.1 -1.1 -0.3 0.0
3.9 3.8 5.0 4.2 3.9
25 14 13 11 0

+1.2 +1.1 -0.6 -0.3 0.0
4.5 4.6 6.3 6.0 5.7
25 12 10 9 0

+2.2 +1.9 -0.3 0.0
5.8 6.1 8.3 8.0
25 12 9 0

+2.3 +1.8 +0.1 -0.6 -0.2 0.0
7.5 8.0 7.7 10.4 10.0 9.8
25 11 8 6 5 3 0

-0.9 -0.6 -0.9 -0.3 0.0
5.2 4.9 5.2 4.6 4.3
25 10 9 7 0

1138.6 1141.9 1142.3 1143.6 1143.7
10.0 6.7 6.3 5.0 4.9
100 30 6.5 6.5 0

+0.1 -1.2 -0.5 -0.8
4.2 5.5 4.8 5.1
10 12 14 25

1151.2 1149.6 1149.8
3.9 5.5 5.3
9 30

-0.4 -1.0 0.0 +1.2
4.6 5.2 4.2 3.0
9 10 12 25

0.0 -0.7 0.0 +1.2 +1.4
3.9 4.6 3.9 2.7 2.5
9 10 20 25

-0.2 -0.5 +1.3 +2.3
5.9 6.2 4.4 3.7
9 10 12 25

-0.4 -0.6 +1.6 +2.2
8.4 8.6 6.4 5.8
10 11 16 25

0.0 -0.5 +0.2 +1.2 +1.7
9.8 10.3 9.9 8.6 8.1
11 13 14 20 25

-0.9 +0.1 -1.1 -0.6 -0.7
5.2 4.2 5.4 4.9 5.0
9 12 13 17 25

1144.1 1144.8 1142.4 1142.6
4.5 3.9 6.2 6.0
8 10 10 30

		1148.56		
280				1143.3
281				1143.4
282				1144.4
283				1142.8
284				1141.1
	0.50	1140.37	8.69	1139.87
285				1138.7
286				1136.2
287				1132.8
288				1129.9
289				1127.5

-1.2	-0.6	-1.1	-0.2	0.0		+0.1	-0.9	-0.5	
6.5	5.9	6.4	5.5	5.3		5.2	6.2	5.8	
25	10	8	6	0		10	12	15-25	
-0.7	-0.7	-1.2	-0.5	0.0		-0.2	-1.0	-0.2	+1.2
5.9	5.8	6.4	5.7	5.2		5.4	6.2	5.4	4.0
25	13	11	9	0		8	9	11-14	18-25
+0.5	+0.3	-0.8	-0.4	0.0	-0.2	-0.7	+0.6	+1.6	+1.8
3.7	3.9	5.0	4.6	4.2	4.4	4.9	3.6	2.6	2.4
25	11	10	8	0	8	9	11	15	30
+0.6	0.0	-0.8	-0.3	0.0		-0.5	-0.9	+0.1	+1.8
5.2	5.8	6.6	6.1	5.8		6.3	6.7	5.7	4.0
25	10	9	7	0		8	9	10	22-30
-0.1	-0.5	-1.0	-0.2	0.0	-0.3	-1.1	+0.3	+0.1	+0.6
7.6	8.0	8.5	7.7	7.5	7.8	8.6	7.2	7.4	6.9
25	10	9	8	0	8	9	10	20	25
+1.7	+0.9	-1.0	-0.3	0.0	-0.4	-1.1	+0.8	+1.5	
0.0	0.8	2.7	2.0	1.7	2.1	2.8	0.9	0.2	
25	15	9	8	0	7	9	11	25	
+1.7	+1.0	-0.1	-1.0	-0.5	0.0	-0.5	-1.0	+0.9	+1.2	+1.7
2.5	3.2	4.3	5.2	4.7	4.2	4.7	5.2	3.3	3.0	2.5
25	15	11	10	9	0	7	8	11	21	25
+2.5	+1.8	+0.5	-0.7	0.0	0.0	-0.5	-1.1	+1.5	+2.7	
5.1	5.8	7.1	8.3	7.6	7.6	8.1	8.7	6.1	4.9	
25	13	11	9	7	0	6	7	11	25	
+2.8	+2.0	+1.0	-0.5	-0.2	0.0	-0.5	-1.1	+1.6	+2.7	
7.7	8.5	9.5	11.0	10.7	10.5	11.0	11.6	8.9	7.8	
25	15	10	9	8	0	7	5	12	25	
+2.5	+1.9	+1.5	-0.3	0.0	0.0	-0.3	-0.9	+0.8	+2.2	
10.4	11.0	11.4	13.2	12.9	12.9	13.2	13.8	12.1	10.7	
25	22	14	9	8	0	6	7	9	25	

		1146.37		
	1.34	1129.65	12.06	1128.31
290				1126.4
290+94	See for Culv. Des. only			1125.2
291				1124.9
292				1123.3
			11.24	11 18.41
293				1121.2
294				1118.9
	6.04	1118.97	10.72	1118.93
295				1116.9
296				1114.9
297				1113.7

+0.9 +0.2 -0.1 -0.9 0.0 0.0 0.0 -0.0 +0.2 -0.2 +0.1
2.4 3.1 3.4 4.2 3.3 3.3 3.3 4.1 3.1 3.5 3.2
25 20 11 10 9 0 6 11 12 15 25

1120.2 1123.3 1123.3 1125.5 1125.2 1126.4 1123.6 1123.8 1124.3 1125.0
9.5 6.4 6.4 4.2 4.5 3.3 6.1 5.9 5.2 4.2
100 30 F.L. 7.5 0 8.5 F.L. 17' F.L. 35

-0.5 -0.6 -1.3 -0.6 -0.2 0.0 +0.1
5.3 5.4 6.1 5.4 5.0 4.5 4.7
25 14 13 11 6 0 25

+0.1 +0.2 -0.9 -0.5 0.0 0.0 -0.2 -0.8 +1.5 +2.5
6.3 6.2 7.3 6.9 6.4 6.4 6.6 7.2 4.9 3.9
25 12 11 9 7 0 8 10 14 25

B.M. Left, 292 +20 (1118.39)

+1.6 +0.7 -1.1 -0.5 0.0 -0.1 -1.0 +1.6 +2.1
6.9 7.8 9.6 9.0 8.5 8.6 7.5 6.9 6.4
25 13 12 10 0 10 12 16 19 25

Fence

+1.5 +0.8 -1.1 -0.7 0.0 -0.5 -1.0 +1.1 +1.4
9.3 10.0 11.9 11.5 10.8 11.3 11.8 9.7 9.4
25 14 12 10 0 9 10 14 25

+1.2 +1.0 +0.5 -1.2 -0.7 0.0 -0.6 -1.3 +0.5 +1.1
0.9 1.1 1.6 3.3 2.8 2.1 2.7 3.4 1.6 1.0
25 23 14 11 10 0 9 11 14 25

+1.4 +1.0 +0.5 -1.0 -0.4 -0.3 0.0 -0.4 -0.6 -1.3 +0.2 +0.9
2.7 3.1 3.6 5.1 4.5 4.4 4.1 4.5 4.7 5.4 3.9 3.2
25 23 14 12 11 7 0 5 9 10 13 25

+0.8 +0.2 -1.2 -0.7 0.0 -0.8 -0.9 -1.5 -0.4 +0.1
4.3 5.1 6.5 6.0 5.3 6.1 6.2 6.8 5.7 5.2
25 14 12 11 0 6 9 10 12 25

		1118.97		
298				1112.0
299				1110.0
300				1107.5
	0.50	1106.76	12.71	1106.26
301				1105.6
302				1103.5
303				1101.6
304				1099.9
304+53				
304+73				
305				1098.0
	1.12	1099.46	8.42	1098.34

+0.8 6.2 / 25 | -0.7 7.7 / 14 | -1.5 8.5 / 13 | -0.7 7.7 / 12 | -0.5 7.5 / 8 | 0.0 7.0 / 0 | -0.5 7.5 / 7 | -1.8 8.8 / 10 | -0.7 7.7 / 12 | -0.4 7.4 / 25

+1.0 8.0 / 25 | -0.7 9.7 / 13 | -1.4 10.4 / 12 | -0.6 9.6 / 11 | 0.0 9.0 / 0 | -0.8 9.8 / 8 | -1.9 10.9 / 10 | -0.7 9.7 / 12 | -0.2 9.2 / 25

+2.0 9.5 / 25 | -0.2 11.7 / 13 | -1.3 12.8 / 12 | -0.4 11.9 / 10 | 0.0 11.5 / 0 | -0.7 12.2 / 8 | -1.6 13.1 / 10 | 0.0 11.5 / 13 | +0.5 11.0 / 25

+1.2 0.0 / 25 | -0.7 1.9 / 12 | -1.3 2.5 / 11 | -0.5 1.7 / 9 | 0.0 1.2 / 0 | -0.5 1.7 / 9 | -1.5 2.7 / 11 | -0.1 1.3 / 12 | -0.2 1.4 / 25

0.0 3.3 / 25 | -0.6 3.9 / 14 | -1.3 4.6 / 13 | -0.3 3.6 / 11 | 0.0 3.3 / 0 | -0.4 3.7 / 7 | -1.1 4.4 / 9 | -0.3 3.6 / 10 | +0.7 2.6 / 25

+0.3 4.9 / 25 | -0.3 5.5 / 14 | -0.9 6.1 / 13 | -0.4 5.6 / 11 | 0.0 5.2 / 0 | -0.5 5.7 / 4 | -1.3 6.5 / 7 | +0.1 5.1 / 9 | +0.9 4.3 / 25

+0.2 6.7 / 25 | +0.1 6.8 / 13 | -0.6 7.5 / 12 | +0.1 6.8 / 11 | 0.0 6.9 / 0 | -0.2 7.1 / 5 | -1.2 8.1 / 7 | -0.1 7.0 / 10 | +0.3 6.6 / 25

1098.2
8.6 / 13 F.L.

1097.3
9.4 / 3.5 F.L.

+0.2 8.6 / 25 | +0.4 8.4 / 13 | +0.1 8.7 / 12 | 0.0 8.8 / 0 | 0.0 8.8 / 3 | -1.2 10.0 / 5 | +0.3 8.5 / 6-9 | +0.9 7.9 / 25

B.M. Left. 305+85 (1098.30)

	1099.46		
306			1097.0
306+61.5			
307			1094.3
308		7.3	1092.2
309		9.3	1090.2

+0.4 −0.6 0.0 −1.5 −0.9 −0.3 +0.7 +1.3

2.1 3.1 2.5 4.0 3.4 2.8 1.8 1.2

25-22 13 0 5 6 8 15 25

1094.0

5.5

16.5

+0.5 −0.4 −1.2 −0.3 0.0 +0.5 1093.3 −1.0 1096.1 1097.4

4.7 5.6 6.4 5.5 5.2 4.7 6.2 3.4 2.1

25 15 14 11 0 16 20 30 100

F.L.

June 1, 1925 Marks, Graw, Reynolds.
Warm - Cloudy.

Culverts

	+	H.I.	−	El.	Gr.
22+20					
	5.1	1234.6		1229.5	
			4.9		1227.7
			9.3		1226.8
29+63					
	5.2	1230.6		1225.4	
			4.4		1224.2
			6.3		1223.3
31+73.7	5.57	1229.55		1223.98	
			2.8		1221.25
			7.8		1217.75
91+82					
	3.41	1269.04		1265.63	
			12.54		1257.0
			4.54		1259.5

Gr. Rod. 1' out side face of H.W.S.

H.W. Stakes, 16.5 Left — 17.5' Right.

℄ El.		
6.9	Cut 2.0'	Stake, 25' L. of ℄.
7.8	Fill 1.5' "	, 25' R. of ℄.

H.W. Stakes, Left, 14.5' Right 15.5'

℄ El.		
6.4	Cut 2.0'	Stake, 25' L. of ℄
7.3	Cut 1.0 "	, 25' R. of ℄

B.M. S.E. of Sisson's Corners

8.30	Cut. 5.5	Stake, 16' Left of ℄ at 32+10
11.80	Cut 4.0	Stake, 16' L. of ℄, 70° S. of Stq 32+10

B.M., Left of 93+20

12.04	Fill 0.3'	Stake on ℄ Barrell, 15' L. of L. End
9.54	Cut 5.0' "	" " " 15' R. of R. End.

95+95	5.0	1264.6		1259.6	
			5.9		1156.7
			6.8		1155.8
110+15					
	5.1	1258.2		1253.1	
			4.5		1250.7
			6.4		1249.8

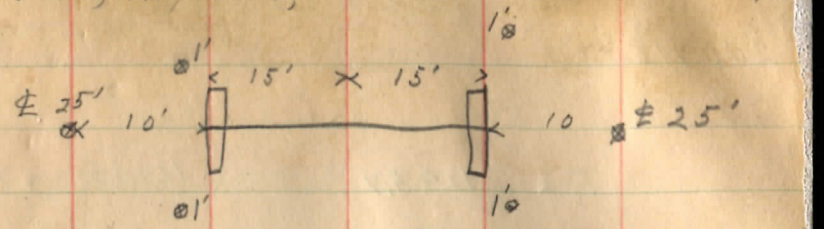
H.W. Stakes. Left, 17.5' Right, 16.5'
El. ℄ of Road.
7.9 Cut 2.0' Stake, 25' R. of ℄.
8.8 C Cut 2.0' " 25' L. of ℄

H.W. Stakes. 16.5' Left. 15.5' Right
El. of ℄ of Road
7.5 Cut 3.0 Stake 25' R. of ℄,
8.4 Cut 2.0' " 25' L of ℄,

July 21, 1925

150+49

5.3	1304.0	1298.7		
			1294.8	
			1295.7	

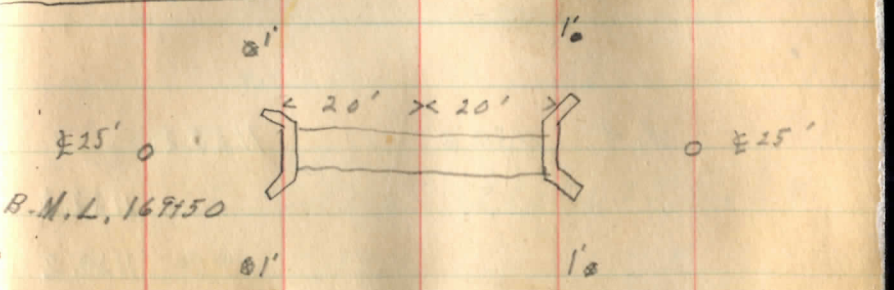


El. ℄ of Rd.

9.2	6.2	Cut 3.0	Stake, 25'L. of ℄
8.3	5.8	Cut 2.5	" " R. of ℄

168+03

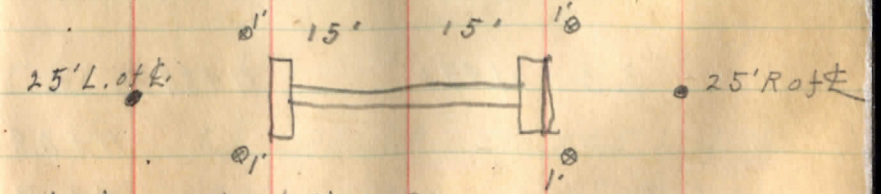
0.60	1286.74	1286.14		
			1273.44	
			1274.06	



13.30	9.30	Cut 4.0	Stake 25'L. of ℄
12.68	9.68	Cut 3.0	" " R " "

192+36

4.60	1263.30	1258.7		
			1256.17	
			1255.33	



El. ℄ of Rd. at Sta. 192+00

7.13	4.63	Cut 2.5'	Stake 25'L. of ℄
7.97	4.97	Cut 5.0'	" " R " "

200+18

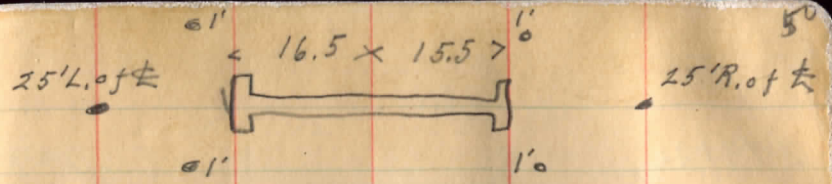
5.2	1245.7	1240.5	
			1236.35
			1237.15

290+94

5.4	1130.6	1125.2	
			1122.3
			1123.2

279+80

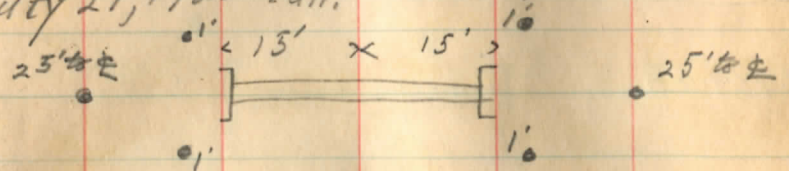
5.3	1149.8	1143.7	
			1140.8
			1141.7



El. of ℄ at 200+18

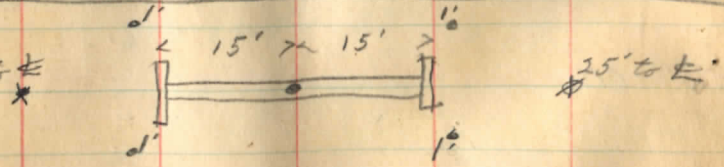
9.35	6.85	Cut 2.5'	Stake 25'L. of ℄
8.55	5.55	Cut 3.0'	" " R. of ℄

July 27, 1925 Fair. Marks-Reynolds-Parks



El. at ℄.

8.3	5.3	Cut 3.0'	Stake 25'L. of ℄
7.4	4.4	Cut 3.0'	" " R. " "



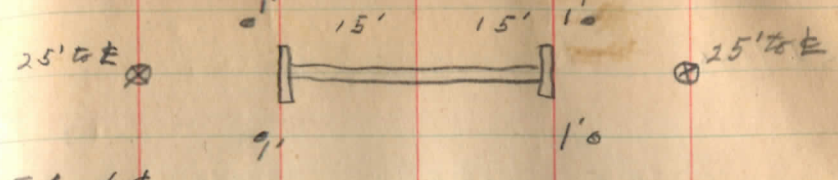
El. at ℄

8.2	5.2	Cut 3.0'	Stake 25'L. of ℄
7.3	5.3	Cut 2.0'	" " R " "

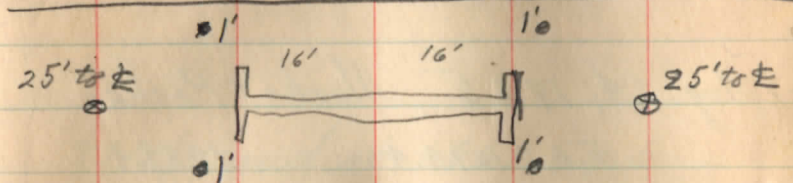
273+22				
	5.3	1156.4	1151.1	
				1148.3
				1149.2

260+63				
	5.3	1158.3	1153.0	
				1149.3
				1150.2

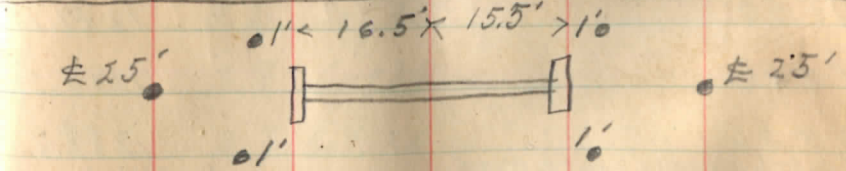
239+00				
	5.2	1189.3	1184.1	
				1178.8
				1179.7



El. at ℄			
8.1	4.1	Cut 4.0	Stake 25' L. of ℄
7.2	5.2	Cut 2.0	" " R. " "



El. at ℄			
9.0	6.0	Cut 3.0	Stake 25' L. of ℄
8.1	6.1	Cut 2.0	" " R. " "



El. at ℄			
10.5	7.5	Cut 3.0'	Stake 25' L. of ℄
9.6	8.6	Cut 1.0'	" " R. " "

229+55

5.2 1205.5 1200.3

1196.6

1197.5

Aug. 24, 1925, Marks + Parks

5.0 1294.4 1289.4

1288.82

7.2 1287.2

Culvert Inlet

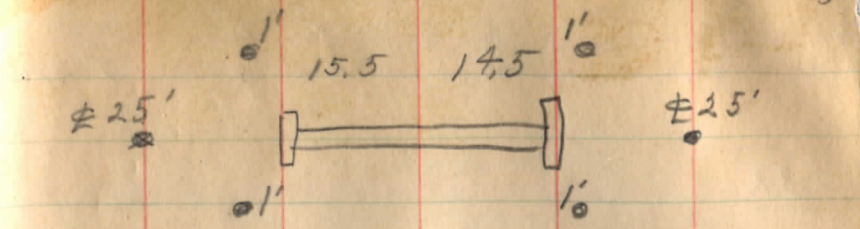
Sta. D+00 1287.2

0+50 1287.7

1+00 1288.2

1+50 1288.7

W. Ditch of Old State Road 157+30 1289.5



El. at ℄.

8.9	6.4	Cut 2.5'	Stake 2.5' L. of ℄
8.0	6.0	Cut 2.0'	" " R " "

℄ of Road at 156+59.5

Grade of Ditch at 157+00

Inlet to Culvert

Grade Rod	Stake	
7.2	4.2	Cut 3.0
6.7	4.2	Cut 2.5
6.2	3.7	Cut 2.5
5.7	3.7	Cut 2.0
4.9	2.9	Cut 2.0

				Grade
282				
	2.65	1156.53	1153.88	
273				1151.55
276				1150.22
277				1148.44
278				1146.66
	6.66	1158.87	4.32 1152.21	
270				1154.40
269				1155.77

Sept. 19, 1925 Marks, Reynolds, Pomeroy
Fair,

stakes set 2' outside slope lines

F0.4 / 20.0 F.0.7 C1.0 / 21.5

B. M. Right 274+15
Grade Rod

4.98	0.0 / 19.5	F.0.2 / 17.5	F0.3 / 0	c.1.0 / 19.3	C1.2 / 21.3
6.31	C.0.5 / 20.4	C,0.4 / 18.4	F.0.8 / 0	c.1.2 / 19.6	C1.5 / 21.6
8.09	C1.1 / 21.5	C1.1 / 19.5	F1.2 / 0	C.0.7 / 18.8	C1.0 / 20.8
9.87	C1.3 / 21.3	C1.0 / 19.3	F1.2	F0.8 / 16.6	F0.4 / 18.6
4.47	0.0 / 19.5	F.0.2 / 17.5	C0.1 / 0	F0.6 / 16.9	F0.4 / 18.9
3.10	C0.6 / 20.5	C0.5 / 18.5	F0.6 / 0	F0.3 / 17.3	0.0 / 19.3

	2.45	1170.27		1167.82	
258+10					1159.65
258					1159.75
257					1163.13
256					1165.90
255+75					1166.50
255					1168.30
	6.40	1175.30	1.37	1168.90	
254					1170.65
253					1172.92
	2.64	1189.33		1186.69	
249					1180.48
248					1184.20
247	9.74	1198.65	0.42	1188.91	1188.60
246					1192.82

B.M. L. of 255+85

10.67				C0.5 / 18.5	C1.2 / 20.5	
10 .32	C1.4 / 21.6	C1.2 / 19.6	F2.5 / 0			
7.14	C1.5 / 21.6	C1.2 / 19.6	F0.9 / 0	C1.4 / 19.9	C1.5 / 21.9	
4.37			F1.1 / 0	C0.6 / 18.7	C0.9 / 20.7	
3.77	F1.0 / 18.0	F1.2 / 16.0		C0.7 / 18.8	C1.0 / 20.8	
1.97	C0.6 / 20.5	C0.5 / 18.5	F1.3 / 0	C1.0 / 19.3	C1.5 / 21.3	
4.65	C2.1 / 22.8	C2.0 / 20.8	F1.1 / 0	C1.3 / 19.7	C1.5 / 21.7	
2 .38	C0.6 / 20.4	C0.4 / 18.4	F0.7 / 0	F0.5 / 17.0	F0.3 / 19.0	

B.M. R. 247+98

8.85	C1.0 / 20.8	C0.7 / 18.8	F1.2 / 0	C0.8 / 18.8	C1.1 / 20.8
5.13	C0.3 / 19.3	F0.3 / 17.3	F1.4 / 0	C0.4 / 18.4	C0.7 / 20.4
0.73	C0.8 / 19.6	F0.1 / 17.6	F2.1 / 0	C1.8 / 20.5	C2.0 / 22.5
5.83	C1.3 / 21.1	C0.9 / 19.1	F1.2 / 0	C0.7 / 18.8	C1.1 / 20.8

		1198.65		
245				1195.98
	7.26	1203.24	2.67	1195.98
244				1198.74
243+65				1198.96
243				1197.76
			4.48	1198.76
	3.32	1202.08		
242				1194.32
241				1190.88
			11.86	
	3.17	1193.39		1190.22
240+25				1188.30

2.67	C 0.0 / 19.5	F 0.2 / 17.3	F 1.2 / 0	F 0.2 / 17.5	C 0.0 / 19.5

T.P. Slope Stake, W. side 245+00

4.50	C 1.1 / 21.0	C 0.8 / 19.0	F 0.9 / 0	C 0.6 / 18.7	C 0.9 / 20.7
4.28	C 1.3 / 21.5	C 1.1 / 19.5	F 0.2 / 0	C 1.0 / 19.3	C 1.2 / 21.3
5.48	C 1.0 / 20.8	C 0.7 / 18.8	F 1.2 / 0	C 0.7 / 18.8	C 1.3 / 20.8

T.P. West. Slope stake 243+00
Sept. 23, 1925, Cool-Fair-Marks-Reynolds

7.76	C 2.9 / 24.0	C. 2.8 / 22.0	F 1.1 / 0	C 1.7 / 20.3	C 1.9 / 22.3
11.20	C 1.4 / 22.0	C 1.5 / 20.0	F 1.6 / 0	C 0.8 / 19.0	C 1.1 / 21.0
5.09	C 1.8 / 22.3	C 1.7 / 20.3	F 2.3 / 0	F 3.0 / 14.8	F 2.8 / 16.8

	2.10	1196.16	1194.06	
237				1189.00
236				1191.50
235				1194.00
	6.51	1201.51	1.16	1195.00
234				1196.50
233				1198.90
	7.54	1206.44	2.61	1198.90
232				1200.56
231				1201.46
230				1201.50
229				1201.72
	7.74	1207.77	6.41	1200.03
228				1203.30
227				1205.00

B.M. R. 236+5 C

7.16	C2.2 / 22.8	C3.0 / 20.8	F1.0 / 0	0.0 / 17.8	0.0 / 19.8
4.66	0.0 / 19.6	F0.1 / 17.5	F1.4 / 0	F0.1 / 17.6	0.0 / 19.6
2.16	C0.8 / 21.0	C0.8 / 19.0	F1.1 / 0	C0.7 / 18.8	C1.0 / 20.8

T.P. Slope Stake, E. 235+00

5.01	0.0 / 19.3	F0.3 / 17.3	F1.4	C0.2 / 18.4	C0.4 / 20.1
2.61	0.0 / 19.5	F0.2 / 17.5	F1.0 / 0	F0.4 / 17.2	19.2
5.88	F0.1 / 19.3	F0.3 / 17.3	F1.2 / 0	F5.0 / 17.0	F0.2 / 19.0
5.04	C0.3 / 19.8	0.0 / 17.8	F0.5	C0.4 / 18.4	C0.6 / 20.4
4.94	F2.0 / 17.0	F2.1 / 15.0	F1.7 / 0	F1.7 / 15.5	F1.5 / 17.5
4.72	F2.0 / 17.0	F2.1 / 15.0	F1.4	F1.8 / 15.0	F1.7 / 17.0

Right Slope Stake, 229+00

4.47	C1.0 / 21.0	C0.8 / 19.0	F1.7 / 0	F1.2 / 16.0	F0.6 / 18.0
2.77	0.4 / 19.3	C0.3 / 17.3	F0.3 / 0	C0.8 / 19.0	C0.8 / 21.0

	5.5	1225.3		1219.8	
214					1220.6
213+75					1220.8
213					1221.0
	1.81	1245.32		1243.51	
204					1241.04
205					1238.17
206					1234.33
	0.78	1236.49	9.61	1235.71	
207					1230.50
208					1226.67
	8.65	1257.61		1248.96	
	8.62	1264.87	1.36	1256.25	
194					1252.25
193+50					1255.37
193					1257.90
			6.16	1258.71	

Sep. 1925 Fair Cool

Marks Reynolds.

℄ Road 213+60

4.7	C0.8 / 20.8	C0.7 / 18.8	F1.1 / 0	C1.9 / 20.6	C1.9 / 22.6
4.5	C1.7 / 22.0	C1.5 / 20.0	C0.7 / 0	C2.1 / 21.0	C2.0 / 23.0
4.3	F1.5 / 18.1		F1.2 / 0	C0.1 / 18.1	C0.7 / 20.1

B.M. Right 204+75

4.28	C2.0 / 22.0	C1.5 / 20.0	C0.1 / 0	C2.5 / 21.5	C3.0 / 23.5
7.15	C1.3 / 21.5	C1.1 / 19.5	F1.0	C2.4 / 20.2	C2.0 / 22.2
10.99	C1.4 / 21.8	C1.3 / 19.8	F0.7 / 0	C2.2 / 21.0	C3.0 / 23.0
5.99	C1.5 / 22.0	C1.4 / 20.0	F1.3 / 0	C2.7 / 21.8	C3.5 / 23.8
9.82			F2.3 / 0	C1.3 / 19.8	C1.7 / 21.8

B.M. Right, 196+45

12.62	C5.4 / 28.0	C5.5 / 26.0
9.50	C5.5 / 27.5	C5.2 / 25.5
6.97	C3.2 / 20.0	

T.P., N.E. cor. E. Headwall, Culvert at 192+50

June 11, 1926 Showers Marks Canfield Goodrich

	9.96	1268.67		1258.71	
192					1260.00
191					1262.01
190					1267.08
	12.12	1280.47	0.32	1268.35	
189					1272.67
188					1278.25
			1.56	1278.91	
	12.98	1291.89			
187					1283.83
186					1289.42
	12.20	1301.37	2.72	1289.17	
185					1293.77
184					1295.67
~~183~~					
183					1296.33
182					1295.73
181					1292.60

T.P.-N.E.Cor., E.H.W. Culvert at 192+50

8.67	F1.6 / 18.0		F1.6 / 17.5
6.66	0.0 / 18.0		F1.9 / 17.5
1.59	C1.3 / 22.5		F1.0 / 19.0
7.89	C3.1 / 24.0		C4.2 / 26.0
2.22	C0.7 / 21.0		C1.8 / 22.0

Rain 3. P.M.

T.P. Stone Hub, Left 188+80
June 16, 1926 Fair. Marks-Canfield.

8.06	C0.9 / 21.5	C2.1 / 21.5
2.47	F0.2 / 20.0	C2.5 / 23.5
7.60	C0.9 / 21.5	C.4.2 / 24.0
5.70	F2.5 / 16.0	F1.6 / 16.0
5.04	F2.5 / 16.0	F2.3 / 16.0
5.64	C1.4 / 23.0	C4.0 / 26.0
8.67	C1.4 / 21.5	C3.0 / 24.0

		1301.37						
180				1288.20	13.17	C2.4 / 22.5		C2.8 / 29.0
	0.74	1291.37	10.74	1290.63				
179				1283.80	7.59	C1.3 / 21.5		C0.6 / 21.0
178				1279.77	4.00	F1.6 / 17.5		F1.3 / 17.5
	2.68	1288.13	12.94	1278.45				
177				1278.52	9.61	F4.1 / 19.5		F2.4 / 16.5
			7.03	1281.10	B.M. Left of 176+50 Elev 1281.13			
176				1280.39	7.74	C1.3 / 21.5		F2.0 / 16.0
	7.58	1295.16	0.55	1287.58				
175				1285.00	12.16	C2.6 / 23.0		C4 / 26.0
174				1289.56	5.60	C1.7 / 22.5		C3.2 / 24.0
173				1291.01	4.15	F0.1 / 19.5		C1.5 / 21.0
172				1289.36	5.80	F0.3 / 19.0		C1.0 / 20.5
171				1287.27	7.89	F0.7 / 18.5		C0.9 / 20.0

		1295.16						
170					1285.18	9.98	0.0 / 20.0	C2.4 / 22.0
	4.87	1291.01		1286.14		B.M. Left 169+50		
169					1283.30	7.71	F0.6 / 21.0	C0.5 / 19.0
168					1282.90	8.11	F4.1 Top of H.W.	F3.5 Top of H.W.
167					1284.21	6.80	C1.8 / 21.5	F1.6 / 17.0
166	6.17	1295.57	1.61	1289.40	1287.00	4.01	C2.4 / 23.0	~~C2.4~~ C3.6 / 24.0
165					1289.68	5.89	C0.5 / 20.0	C2.1 / 21.0
164					1291.70	3.87	C0.3 / 19.5	C1.0 / 20.5
	1.56	1305.43		1301.87		B.M. Right, 160+05		
161					1296.80	6.63	F1.0 / 18.0	F0.9 / 18.0
160					1297.45	5.98	C2.9 / 24.0	C3.7 / 25.0
159					1296.00	7.43	C1.1 / 21.5	C2.0 / 22.5

	6.2	1303.6		1297.4		± rd		151+00		
151					1298.0	5.6				C0.9 / 20.5
152					1294.6	9.0	C1.4 / 21.5			C1.0 / 20.0
	7.12	1300.17		1293.05		B.M.	right,	135+35		
139					1297.60	2.57				C0.8 / 20.5
138+50					1297.70	2.47	F0.4 / 20.0			C1.2 / 20.0
138					1297.20	2.97	F0.1 / 18.0			C2.3 / 22.5
137					1295.60	4.57	C0.5 / 20.0			
	0.81	1293.86		1293.05		B.M.	right	135+35		
133					1287.59	6.27	C1.1 / 21.5			C0.6 / 18.0
132					1283.30	10.56	C1.7 / 21.0			C1.1 / 20.0
131					1278.84	15.02	C5.7 / 27.5			C1.0 / 21.0
	1.21	1283.18	11.89	1281.97						

		1283.18			
130					1274.38
129	0.84	1273.36	10.66	1272.52	1269.92
					~~1265.6~~
128					1265.63
			6.71	1266.65	
	0.27	1266.90		1266.63	
	11.05	1272.21	5.74	1261.16	
122					1265.1
121					1267.48
120					1268.71

8.80	F1.5 / 17.0		C2.6 / 22.5
13.26	F1.7 / 18.0		C2.6 / 22.5
7.73	F1.8 / 17.5		C4.3 / 25.0

B.M. right 127+35 (1266.63 rec)

N.W. cor. - W.H.W. culv. at 125+45

7.07	F1.4 / 17.5	C1.0 / 21.0
4.73	F0.9 / 18.0	C1.7 / 21.5
4.00		C1.1 / 20.0

July 1, 1926, Fair — Marks - Canfield

	0.46	1188.13		1187.67		B.M. Stapte, N. E. root, Elm, S.W. of Lampman's Cor.
2					1182.00	6.13 — F0.7 / 18.5 — F1.1 / 22.0
3					1179.50	8.63 — C2.3 / 23.0 — C1.6 / 21.5
~~4~~	4.94	1181.08	11.99	1176.14	~~1176.00~~	
4					1176.00	5.08 — F0.4 / 20.5 — C.3.3 / 24.0
5					1172.00	9.08 — F2.0 / 16.5 — F3.1 / 18.0
	4.55	1175.19	10.44	1170.64		
6					1170.50	4.69 — F3.6 / 17.0 — F3.3 / 17.0
7					1171.50	3.69 — F3.8 / 17.5 — F3.0 / 17.0
8					1172.50	2.69 — F2.1 / 16.0 — F2.4 / 16.0
9					1173.50	1.69 — F1.3 / 17.5 — F0.2 / 19.0
	10.32	1185.14	0.37	1174.82		
10					1175.92	9.22 — C1.5 / 21.5 — C0.9 / 20.5

		1185.14						
11				1181.20	3.94	C2.1 / 22.5		C1.4 / 19.0
	10.27	1194.62	0.79	1184.35				
12				1187.90	6.72	C1.8 / 21.5		C1.4 / 23.0
	10.78	1204.71	0.69	1193.93				
13				1194.60	10.11	C1.9 / 21.5		F0.1 / 18.0
14				1201.30	3.41	C1.9 / 21.5		F1.4 / 14.0
	9.89	1214.58	0.02	1204.69				
15				1207.32	7.26	C2.1 / 22.0		F0.1 / 19.0
16				1211.75	2.83	C3.1 / 22.5		C2.0 / 20.0
	6.52	1221.10	0.00	1214.58				
17				1215.50	5.60	C2.2 / 22.5		F0.1 / 19.5
			1.85	1219.25		B.M. Left, 17+20 Rec.		
18				1219.25	1.85	C3.5 / 23.0		F1.8 / 17.5
	11.91	1232.89	0.12	1220.98				
19				1222.69	10.20	C1.1 / 21.0		F1.1 / 17.0
20				1225.50	7.39	C1.2 / 21.0		0.0 / 19.0

		1232.89							
21					1228.00	4.39	C 1.7 / 21.5	C 1.2 / 21.5	
22					1230.98	1.91	F 1.3 / 17.5	F 2.9 / 16.0	
	11.09	1243.37	0.61	1232.28					
23					1234.90	8.47	F 1.8 / 16.0	F 2.5 / 16.0	
24	3.32	1243.75	2.94	1240.43	1239.30	4.07	C 2.4 / 23.0	C 1.1 / 21.0	T.P. on Right Slope Hub.
+50					1240.55	3.20	C 2.1 / 22.5	C 0.6 / 20.0	
25					1239.88	3.87	C 0.6 / 20.5	F 1.6 / 17.0	
26					1236.63	7.12	C 2.2 / 22.0	C 0.4 / 19.5	
27					1233.38	10.37	C 0.8 / 21.0	F 1.1 / 18.0	
	3.98	1235.63	12.00	1231.65					
28					1230.13	5.50	C 0.2 / 19.0	F 1.6 / 19.0	
29					1227.67	7.96	F 0.1 / 18.0	F 1.1 / 17.5	
	3.17	1230.60	8.20	1227.43					
30					1226.00	4.60	0.0 / 19.5	F 1.4 / 17.5	

		1230.60			
31					1224.33
			6.60	1224.00	
	7.52	1231.50		1223.98	
32					1224.33
33					1228.50
34	12.77	1242.72	1.55	1229.95	1232.67
35					1236.83
36	7.34	1248.29	1.79	1240.95	1240.32
37					1242.43
38					1243.87
	8.14	1273.77		1265.63	
94					1265.40
93					1267.25
92					1267.75
91	12.40	1281.55	4.62	1269.15	1270.20
90					1274.60
89					1278.35

6.27 C1.5 / 19.5 — C0.9 / 20.5

B.M. 2nd Tree on E. side S. from Sissons Cor. (1223.98 TEC)

July 3, 1926, Cloudy — Marks, Parks - Canfield

B.M.

7.17 C0.8 on H.W.

3.00 C 3.1 / 24.0 — C 1.5 / 21.0

10.05 C 3.7 / 24.5 — C 2.1 / 22.0

5.89 C 3.0 / 24.0 — C 1.6 / 21.0

7.95 C 2.0 / 22.0 — C 0.6 / 20.0

5.84 C 2.0 / 22.0 — C 0.5 / 20.0

4.40 C0.5 / 20.0 — 0.0 / 20.0

B.M., L 93+20 — July 9, 1926, Hot, Sprinkles — Marks Canfield

8.27 C0.2 / 19.5 — C 3.0 / 23.5

6.51 0.0 / 20.0 — C 2.9 / 23.0

7.02 F5.0 on H.W.

3.57 F0.6 / 17.5 — F1.1 / 17.5

6.95 C 3.5 / 25.0 — C 2.3 / 22.0

3.20 C 1.5 / 21.5 — C0.7 / 20.0

July 10, 1926 Showers, Marks, Grau, Canfield

	1.92	1267.55		1265.63	
97	9.06	1272.78	3.83	1263.72	1263.40
98					1267.43
99					1268.83
100					1267.60
101					1265.52
	2.29	1269.89	5.18	1267.60	
102					1262.50
103	2.08	1262.81	9.16	1260.73	1259.00
104			~~9.16~~		1255.50

B. M. L. 93+20

4.15	F2.4 / 16.0	C3.0 / 20.0
5.35	C0.6 / 20.0	C2.3 / 22.0
3.95	0.0 / 19.5	0.0 / 19.5
5.18	F1.4 / 17.5	F0.6 / 18.5
7.26	C0.3 / 19.5	C2.1 / 22.0

Slope Stk. R. 101+00

7.39	C0.5 / 19.5	C1.0 / 20.5
10.89	C1.1 / 21.5	C1.7 / 22.0
7.31	C0.8 / 21.0	C0.9 / 21.5

Profile of Sub-Grade

July 26, 1926
Warm, N.E. Wind

Marks - Canfield.

B.M. R. 236 + 50

	2.12	1196.18		1194.06	
235			3.2	1193.0	1194.00
236			5.9	1190.3	1191.50
237			8.1	1188.1	1189.00
	4.99	1192.90	8.27	1187.91	
238			7.3	1185.6	1186.50
239			7.9	1185.0	1185.48
240			6.4	1186.5	1187.44
241			2.5	1190.4	1190.88
	10.20	1200.94	2.16	1190.74	
242			7.0	1193.9	1194.32
243			3.8	1197.1	1197.76
+65			3.1	1197.8	1198.96
244			3.6	1197.3	1198.74
245			5.7	1195.2	1195.98
246			8.8	1192.1	1192.82
	0.18	1192.67	8.45	1192.49	
247			4.7	1188.0	1188.60
			5.94	1186.73	
248			9.0	1183.7	1184.20

B.M. R. 247+90 (1186.69)

		1192.67			
	1.26	1183.43	10.50	1182.17	
249			3.4	1180.0	1180.48
250			5.8	1177.6	1178.10
251			7.7	1175.7	1176.40
252			9.3	1174.1	1174.70
253			11.1	1172.3	1172.92
				1172.98	
	0.30	1173.28	10.45	~~2~~	
254			3.3	1170.0	1170.65
255			5.9	1167.4	1168.30
256			8.2	1165.1	1165.90
	1167.82				~~B.M. L. 255+~~
	5.40				
	1173.22		5.40	1167.88	B.M. L. 255+85 (1167.82)
257			10.9	1162.3	1163.13
	0.97	1162.90	11.29	1161.93	
258			3.7	1159.2	1159.95
259			6.9	1156.0	1156.58
260			9.4	1153.5	1154.38
261			10.5	1152.4	1153.58
262			10.2	1152.7	1154.18
~~2~~	5.88	1160.61	8.17	1154.73	

1160.61

263	6.1	1154.5	1155.92
264	4.9	1155.7	1157.25
265	3.7	1156.9	1157.92
266	3.9	1156.7	1157.92
267	4.5	1156.1	1157.33
268	4.8	1155.8	1156.67

	+	H.I.	−	El.
B.M.	0.24	1187.91		1187.67
0+00			3.1	1184.8
+40			3.3	1184.6
1			5.0	1182.9
2			6.8	1181.1
+60			8.1	1179.8
+94			8.1	1179.8
3			8.3	1179.6
4			13.0	1174.9
		1177.53		
	2.52	~~1179.01~~	12.90	1175.01
5			6.6	1170.9
+55			7.0	1170.5
+74			7.3	1170.2
6			8.0	1169.5
7			7.8	1169.7
8			7.0	1170.5
9			5.4	1172.1
10			2.1	1175.4
	9.65	1186.79	0.39	1177.14

Aug. 13, 1926, Warm-Cloudy Marks - P[illegible] Schofield

		1231.70		
	10.74	1234.57	7.87	1223.83
32			10.3	1224.3
33			6.1	1228.5
34			2.3	1232.3
	9.87	1243.59	0.85	1233.72
35			7.3	1236.3
36			3.9	1239.7
37			2.2	1241.4
38			0.3	1243.3
B.M.	8.71	1291.82		1283.11
61			11.3	1280.5
62			8.7	1283.1
63			5.5	1286.3
64			1.5	1290.3
	9.44	1300.75	0.51	1291.31
65			7.3	1293.4
66			4.4	1296.3
67			1.4	1299.3
	11.45	1311.28	0.92	1299.83

	+	1186.79	−	
11			6.5	1180.3
12			0.3	1186.5
	11.54	1198.05	0.28	1186.51
13			4.7	1193.3
	9.90	1207.64	0.31	1197.74
14			7.1	1200.5
+25			5.5	1202.1
15			1.6	1206.0
	12.25	1219.63	0.26	1207.38
16			8.7	1210.9
17			5.0	1214.6
Rec. 1219.21 B.M.,		1219.21 1219.55 34	0.34	1219.21
+40			3.7	1215.8
+80			1.8	1217.7
18			1.3	1218.2
	10.87	1230.01	0.41	1219.14
19			8.5	1221.5
20			5.5	1224.5
21			2.5	1227.5

1311.28

68			9.8	1301.5
69			7.9	1303.4
70			6.4	1304.9
71			4.8	1306.5
72			3.1	1308.2
73			1.5	1309.8
74			1.2	1310.1
75			0.9	1310.4
	2.58	1313.31	0.55	1310.73
76			3.0	13103
77			3.8	1309.5
78			5.2	1308.1
79			7.0	1306.3
1309.07 B.M.			4.26	1309.05
80			9.8	1303.5
	1.28	1303.12	11.47	1301.84
81			3.7	1299.4
82			8.2	1294.9
83			12.2	1290.9
	0.34	1291.11	12.35	1290.77

Line O.K

		1230.01			
	11.66	1241.08	0.59	1229.42	
22			10.8	1230.3	
23			7.8	1233.3	
+25			6.9	1234.2	
+50			5.7	1235.4	
+75			4.3	1236.8	
24			2.9	1238.2	
+25			2.2	1238.9	
+50			1.7	1239.4	
+75			2.0	1239.1	
25			2.6	1238.5	
26			5.0	1236.1	
27			8.8	1232.3	
28			11.9	1229.2	
	2.62	1231.70	12.00	1229.18	
29			4.7	1227.0	
30			6.3	1225.4	
31			7.3	1224.4	
+73			8.5	1223.2	
1223.98 B.M.			7.72	1223.98	

		1291.11			
84			3.6	1287.5	2' E
85			5.8	1285.3	4' E
86			7.4	1283.7	Grade is Built 5' E of proper Loc'n
87			9.5	1281.6	6' E.
88			11.1	1280.0	5' E
	2.59	1281.41	12.29	1278.82	
89			4.2	1277.2	2½' E.
90			7.8	1273.6	Line O.K.
91			11.9	1269.5	
	2.48	1271.73	12.16	1268.25	
+50			3.6	1268.1	
92			4.6	1267.1	
93			5.5	1266.2	
1265.63 B.M.			6.10	1265.63	
94			7.2	1264.5	
95			10.3	1261.4	
96			10.9	1260.8	
97			9.0	1262.7	
	8.30	1271.64	8.39	1263.34	
98			5.0	1266.6	

		1271.64		
98+50			3.8	1267.8
99			3.9	1267.7
100			5.0	1266.6
+50			5.6	1266.0
101			6.7	1264.9
102			9.8	1261.8
	1.52	1262.81	10.35	1261.29
103			4.4	1258.4
104			8.4	1254.4
105			10.8	1252.0
106			11.5	1251.3
107			11.1	1251.7
Aug. 17 - Cloudy - Marks, Parks - Canfield				
B.M., right. 127+35	1.29	1267.92		1266.63
119			1.6	1266.3
120			0.5	1267.4
121			1.3	1266.6
122			3.5	1264.4
122+50			4.3	1263.6

	+	H.I.	−	El.
123			6.0	1261.9
124			7.6	1260.3
125			8.0	1259.9
+~~70~~ 39			7.5	1260.4
+50			7.5	1260.4
+67			7.7	1260.2
126			7.5	1260.4
127			6.4	1261.5
+34			5.6	1262.3
128			2.9	1265.0
B.M., Right 127+35	10.08	1276.71		1266.63
129			9.5	1267.2
130			3.4	1273.3
B	12.94	1289.36	0.29	1276.42
131			11.4	1278.0
132			6.7	1282.7
133			2.6	1286.8
+55			0.8	1288.6
	11.28	1300.09	0.55	1288.81

	+		-	
		1300.09		
134			10.5	1289.6
135			8.8	1291.2
BM		1293.05 + 7.13 = 1300.18	7.13	1292.96
136			7.2	1292.9
137			5.3	1294.8
138			3.7	1296.47
+50			3.1	1297.0
139			3.5	1296.6
140			4.3	1295.8
141			4.8	1295.3
+35			4.4	1295.7
+61			3.8	1296.3
	8.78	1306.47	2.40	1297.69
142			10.6	1295.9
143			9.7	1296.8
144			7.5	1299.0
+45			6.2	1300.3
145			3.6	1302.9
+16			2.6	1303.9

+27		1306.47	1.2	1305.3
+39			1.0	1305.5
+45			2.0	1304.5
+83			4.2	1302.3
146			4.4	1302.1
BM			3.32	1303.15
B.M.	3.32	1306.55		1303.23
147			5.4	1301.15
148			5.8	1300.75
149			6.6	1299.95
150			7.8	1298.75
	2.04	1300.77	7.82	1298.73
151			3.6	1297.2
+50			4.7	1296.1
152			6.7	1294.1
153			10.8	1290.0
154			12.4	1288.4
+50			12.9	1287.9
~~60~~	5.24	1294.36	11.65	1289.12
+61			6.4	1288.0

		1294.36		
155			6.3	1288.1
156			5.3	1289.1
157			3.9	1290.5
158			1.3	1293.1
	10.20	1303.46	1.10	1293.26
159			7.7	1295.8
+35			7.0	1296.5
160			6.6	1296.9
+50			6.5	1297.0
B.M. 1301.87 Pecanwood			1.58	1301.88
161			7.4	1296.1
162			9.0	1294.5
163			10.7	1292.8
164			12.2	1291.3
	1.88	1292.74	12.60	1290.86
165			3.6	1289.1
166			5.9	1286.8
167			8.9	1283.8
167+50			9.9	1282.8

		1292.74		
168			10.2	1282.5
169			9.4	1283.3
170			7.9	1284.8
B.M. 1286.14 L. 169+50			6.56	1286.18
	6.34	1292.48		1286.14
171			5.5	1287.0
172			3.9	1288.6
173			2.0	1290.5
+50			2.5	1290.0
174			3.7	1288.8
+67			6.1	1286.4
175			8.1	1284.4
+35			10.2	1282.3
176			12.3	1280.2
B.M. 1281.13 L. 176+50			11.32	1281.16
	6.85	1287.98		1281.13
176+50			9.3	1278.7
177			9.7	1278.3
+50			9.5	1278.5
178			8.5	1279.5

		1287.98		
178+68			6.5	1281.5
~~179~~				
179			5.0	1282.0
	10.58	1298.41	0.15	1287.83
+35			14.1	1284.3
180			10.4	1288.0
+24			9.2	1289.2
+50			8.2	1290.2
181			6.3	1292.1
+50			5.0	1293.4
182			3.3	1295.1
+50			3.0	1295.4
183			2.9	1295.5
+50			3.0	1295.4
184			3.6	1294.8
+50			4.1	1294.3
185			5.3	1293.1
+50			7.5	1290.9
	1.44	1289.50	10.35	1288.06
186			1.4	1288.1

		1289.50		
186+62			4.3	1285.2
187			6.5	1283.0
188			12.3	1277.2
	0.59	1278.06	12.03	1277.47
189			6.3	1271.8
190			11.7	1266.4
	0.99	1266.78	12.27	1265.79
+75			4.2	1262.6
191			5.4	1261.4
+32			6.7	1260.1
192			8.2	1258.6
+38			8.6	1258.2
193			10.4	1256.4
	0.89	1255.10	12.57	1254.21
+36 ~~+50~~			0.1	1255.0
+50			1.0	1254.1
194			4.0	1251.1
+50			6.6	1248.5
195			8.4	1246.7

		1		1245.4
		9.		1245.2
		10.3		1244.8
196			1248.96	
E. M. 1248.96			6.10	
at J. Carvers.			1255.02	
	3.30	1247.47	10.85	1244.17
197			1.4	1244.1
198			3.8	1243.7
199			5.6	1241.9
200			6.2	1241.3
200+30			6.4	1241.1
201			6.3	1241.2
202			6.2	1241.3
	3.58	1244.74	6.31	1241.16
203			3.5	1241.1
203+70			3.4	1241.3
4-			4.1	1240.6
204+70		1243.51	1.18	1243.56
205		1.18	7.0	1237.7
		1244.69		
			10.7	1234.0
	1.34	1233.26	12.77	1231.92
		11		

			3.32	
207			3.2	12
208			3	1220.6
209			3	1223.1
+95			12.9	1220.4
210			13.1	1220.2
+16			13.4	1219.9
	3.91	1224.08	13.10	1220.16
211			4.8	1219.3
212			4.4	1219.7
213			4.1	1220.0
+55			3.9	1220.2
214			4.5	1219.6
215			5.9	1218.2
216			7.6	1216.5

Aug. 25, 1920, P.M. Mr. R. L. Snyder

FRENCH DRAIN LOCATION

5+20	20'	Right	Square →
~~5+36~~	~~[illegible]~~	~~[illegible]~~	~~→~~

Shingledecker

150	4.985
148.	3.300
Diff.	1.685
148	3.440
	5.125

Table IX.—C[illegible] of Ear[illegible]

HEIGHT

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.04	.08	.06	.08	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.07	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.11	.11	.17	.22	.27	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.15	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.19	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.93	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.2	70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.3	6	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.93	1.39	5	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.9	.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.0	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.	.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	.7	1.61	2.	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	.8	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.5	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.1	1.8	2.	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.2	1.8	2.	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.2	1.8	2.52	3.15	3.78	4 40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.3	1.9	2.	3.24	3	4.53	5.18	5.82	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.0	2.67	3.33	4.	5	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.69	1.37	2.06	2.74	3.42	4.1	9	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.1	2.	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	89	3.61	4 33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.9	3.7	.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table give[illegible] cu. yds. in 1 ft. of a trian[illegible] f given width and height. Corrections for [illegible] f w[illegible]h are one tenth the value [illegible] under each height considering the widths from [illegible]s tenths [illegible]similarly the [illegible]s for tenths of height are one tenth the figures op[illegible]e widt[illegible] dering the he[illegible]om 1 to 9 as tenths. Thus if w =16.2 and [illegible] cu. yds. =1.4 [illegible]+.089 =1.597 [illegible]ds. or practically 160 cu. yds. per 100 ft. [illegible]ds 40 ft [illegible] half and multiply result by 2, if both w and h are large use [illegible] half of ea[illegible] multiply result by 4. Any cross-section may be divided into t[illegible]gles b[illegible]th[illegible]wing rule. To the triangle of the sum of the outside cuts (or fills) [illegible]h and [illegible]e [illegible]bed =w, add the triang[illegible]s formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) [illegible]ting the outer from the inner.

[illegible]STANCES FROM CL[illegible] OF ROADWAY FOR [illegible] CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes [illegible] on 1½.

[illegible]de Track Embankm[illegible]

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	[illegible]	[illegible].2	[illegible]	[illegible]
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	[illegible]	[illegible]
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	[illegible]	[illegible]
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	[illegible]	[illegible]
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	[illegible]	[illegible]
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	[illegible]	[illegible]
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	[illegible]	[illegible]
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	[illegible]	[illegible]
8	20.0	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
9	21.5	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	22.9	[illegible]
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	[illegible]	[illegible]
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	[illegible]	[illegible]
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	[illegible]	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	[illegible]	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	[illegible]	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	[illegible]	31.7	[illegible]	[illegible]
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	[illegible]	33.2	33.4	[illegible]
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	[illegible]	34.7	34.9	[illegible]
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	[illegible]	36.2	[illegible]	[illegible]
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	[illegible]	[illegible].7	[illegible]	[illegible]
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	[illegible]	39.2	[illegible]	[illegible]
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	[illegible]	40.7	40.[illegible]	[illegible]
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	[illegible]	42.2	[illegible]	[illegible]
23	42.5	42.7	42.8	43.0	43.1	43.3	43.[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	[illegible]	[illegible]	[illegible]	[illegible]
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	[illegible]	[illegible]	[illegible]	[illegible]
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	[illegible]	[illegible]	[illegible]	[illegible]
27	48.5	48.7	48.8	49.0	49.1	49.3	[illegible].4	[illegible]	[illegible]	[illegible]	[illegible]
28	50.0	50.2	50.3	50.5	50.6	50	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
29	51.5	51.7	51.8	52.0	52.1	52	[illegible].4	52.6	[illegible].7	[illegible]	[illegible]
30	53.0	53.2	53.3	53.5	53.6	53.[illegible]	53.9	54.[illegible]	54.2	[illegible]	[illegible]
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	[illegible]	[illegible]	[illegible]
32	56.0	56.2	56.3	56.5	56.6	56.8	56[illegible]	57.1	57.[illegible]	5[illegible]	[illegible]
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	[illegible]
34	59.0	59.2	59.3	59.5	59.[illegible]	59.8	59.9	60.1	60.2	60.4	[illegible]
35	60.5	60.7	60.8	61.0	61.[illegible]	61.3	61.4	61.6	61.7	[illegible].9	[illegible]
36	62.0	62.2	62.3	62.5	62.[illegible]	[illegible].8	62.9	63.1	63.2	[illegible]	36
37	63.5	63.7	63.8	64.0	64.[illegible]	[illegible].3	64.4	[illegible]	64.7	[illegible].9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	[illegible]	66.2	66.[illegible]	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	[illegible]	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	[illegible]	[illegible].4	40

Example—If point is 22.6 ft. above grade, how far should it be f[illegible] [illegible] to be a slope stake point? Ans. from Table 41.9. For same slopes [illegible] roadbed correct above figures by one-half difference in width of road[illegible] above for 20 ft. roadbed d[illegible]stance will be 41.9—(20—16)÷2 or 2 ft[illegible] [illegible].9—39.9. For slopes of 1 on 1 see [illegible]ide of front cov[illegible]